Duarte Gonçalves Galhardo

Bachelor of Science in Environmental Engineering

Tools to Predict Road Runoff Pollution

Dissertation to obtain Master Degree in Environmental Engineering

Supervisor: João Nuno Fernandes, Postdoctoral Research Fellow, LNEC
Co-Supervisor: Pedro Santos Coelho, Assistant Professor, FCT NOVA

Jury:
President: Leonor Miranda Amaral, Assistant Professor, FCT NOVA
Examiner: Ana Estela Barbosa, Assistant Researcher, LNEC
Supervisor: João Nuno Fernandes, Postdoctoral Research Fellow, LNEC

FACULDADE DE
CIÊNCIAS E TECNOLOGIA
UNIVERSIDADE NOVA DE LISBOA

December, 2018

Duarte Gonçalves Galhardo
Bachelor of Science in Environmental Engineering

Tools to Predict Road Runoff Pollution

Dissertation to obtain the Master's Degree in Environmental Engineering

Supervisor: João Nuno Fernandes, Postdoctoral Research Fellow, LNEC
Co-Supervisor: Pedro Santos Coelho, Assistant Professor, FCT NOVA

Jury:
President: Leonor Miranda Amaral, Assistant Professor, FCT NOVA
Examiner: Ana Estela Barbosa, Assistant Researcher, LNEC
Supervisor: João Nuno Fernandes, Postdoctoral Research Fellow, LNEC

Faculty of Sciences and Technology

NOVA University of Lisbon

December, 2018

Tools to Predict Road Runoff Pollution

Agradecimentos

Este trabalho representa o culminar dos últimos cinco anos da minha vida. Resta-me agradecer, desta forma singela, às pessoas que nele estiveram presente com quem tive não só o prazer trabalhar mas também de criar amizades.

Ao Laboratório Nacional de Engenharia Civil (LNEC), pela oportunidade de integrar um grupo e uma instituição tão prestigiada e que tanto me ensinou neste período.

Ao Engenheiro João Fernandes, pela orientação de trabalho ao longo deste tempo, mas também pela amizade e forma como me acolheu nesta etapa da minha vida.

Ao Professor Pedro, por me ter dado esta oportunidade, mas também por aquilo que representou ao longo do curso. Mais do que um Professor, uma ajuda constante e sempre disponível para ouvir. Quaisquer palavras ficarão aquém. Obrigado por tudo!

À Engenheira Ana Estela Barbosa, pela oportunidade de desenvolver o meu trabalho no âmbito de um projeto tão interessante.

Ao grupo de colegas do LNEC, pelo companheirismo e motivação ao longo de todos estes meses.

À minha família, por serem imprescindíveis. Vocês sabem o quanto são valiosos e o quanto a minha vida se baseia em tudo aquilo que me ensinaram e ensinam dia a dia. Nada disto era possível, nem valeria a pena sem vocês. São tudo para mim!

À Sara, por mais do que uma ajuda constante nesta tese, me aturar no último ano. Obrigado por estares sempre ao meu lado e seres a minha maior confidente e melhor amiga.

À Pipa, ao Marco, à Bela e ao Zé Duarte, pela amizade e apoio nesta fase da minha vida.

Aos meus amigos de Arraiolos por estarem presentes mesmo após largos meses de ausência.

Aos amigos que a grande FCT me deu. Esta faculdade só se tornou tão grande e tão especial na minha vida, hoje e sempre, devido à vossa presença. Obrigado pela cumplicidade, pela amizade, pelas noites de estudo e por tudo aquilo que já vivemos e iremos viver, juntos.

OBRIGADO POR TUDO!

Abstract

The concern about the environment is constantly increasing. The conservation of water resources is among the major issues. If previously the major concern with this resource was only the quantitative level, nowadays the qualitative level is a concern equally important.

Taking into account this major concern and due to the increasing urban development, road runoff has become a growing issue since it is a potential form of diffuse pollution. Because of the relevance of this source of pollution, road operators and environmental agencies have developed new models for road runoff prediction. In this dissertation, four of these models were assessed: PREQUALE (Portugal), Highways Agency Water Risk Assessment Tool (HAWRAT - UK), Kayhanian's model (USA) and Stochastic Empirical Loading and Dilution Model (SELDM - USA).

After a literature review on this subject, the study started with the collection of monitored data from 20 roads in six European countries. For each road, the Site Mean Concentrations (SMC) were calculated for total suspended solids (TSS), copper, zinc, lead and cadmium. From these the SMC of TSS were above the emission limit declared by the Portuguese regulation (Decree-Law 236/98, from 01 of August) for some of the roads.

The second step was the evaluation of the four prediction models, through the comparison between monitored data and model results. Together with the visual observation, four error indices were calculated to check which model was best adapted to the European monitored data. It was verified that none of the models presents sufficiently robust values to be used like a general model of application to the whole Europe.

Furthermore, a new prediction equation was developed. This equation was calibrated with data from all Europe, unlike the four previous models, which were calibrated for a country or region. As whole data were used to calibrate the model, the results agree with the data. Nevertheless, its use in real and different roads should be carefully assessed.

Keywords: Road runoff, PREQUALE, HAWRAT, Kayhanian's model, SELDM, SMC

Resumo

Os recursos hídricos têm apresentado cada vez maior importância, havendo uma transformação na consciência coletiva, sendo que inicialmente a importância deste recurso era essencialmente quantitativa e agora é igualmente qualitativa.

Tendo em conta este facto, as escorrências rodoviárias tornaram-se uma preocupação cada vez maior, visto constituírem uma potencial fonte de poluição difusa. Tendo em conta esta premissa, as agências rodoviárias e do ambiente têm desenvolvido novos modelos de previsão de escorrências rodoviárias. Neste trabalho foram estudados quatro modelos: PREQUALE (Portugal), *Highways Agency Water Risk Assessment Tool* (HAWRAT do Reino Unido), um modelo de Kayhanian (EUA) e *Stochastic Empirical Loading and Dilution Model* (SELDM dos EUA).

Primeiramente foram recolhidos dados monitorizados de 20 estradas de seis países europeus sendo posteriormente calculadas as concentrações médias do local (CML) para cada uma das estradas. Foi possível verificar que apenas a CML de sólidos suspensos totais para algumas estradas se encontra acima do limite de emissão de águas residuais consignado no Decreto-Lei n.º 236/98, de 01 de agosto, estabelecendo-se assim uma análise das CML a nível europeu.

Posteriormente, foi feita uma avaliação dos quatro modelos estudados. Para cada uma das 20 estradas foi estudado qual o modelo que melhor se adaptava aos resultados de monitorização, através de uma análise visual e de erros calculados. Verificou-se que nenhum dos modelos apresenta valores suficientemente robustos para ser utilizado como modelo geral de aplicação a toda a Europa.

Tendo a análise dos quatro modelos em conta, foi desenvolvida uma equação de previsão, que foi calibrada com os dados das 20 estradas europeias, ao contrário dos quatro modelos anteriormente referidos, que foram calibrados para um determinado país ou região desse país. Os resultados não foram considerados suficientemente robustos, para permitir a utilização deste modelo à escala europeia, mas foram bastante melhores que os obtidos através dos outros modelos, tendo em conta que o modelo foi aplicado às estradas que permitiram a sua calibração. O uso deste modelo em novas estradas deve ser objeto de uma análise bastante cuidada.

Palavras-Chave: Escorrências rodoviárias, PREQUALE, HAWRAT, modelo de Kayhanian, SELDM, CML.

List of Contents

List of figures

List of tables

Acronyms and glossary

AADT	Annual average daily traffic
AADTC	Annual average daily traffic constant
ADP	Antecedent dry period
ANN	Artificial neural network
AR	Annual average rainfall volume with the same duration as the basin concentration
BDF	Basin development factor
C_p	Estimated concentration for the pollutant p
COD	Chemical oxygen demand
CR	Climate region
CRC	Climate region constant
CRM	Coefficient of residual mass
CSR	Cumulative seasonal rainfall
DA	Drainage area
DL	Drainage length
EMC	Event mean concentration
E_{NS}	Efficiency Nash-Sutcliffe coefficient
GUI	Graphical user interface
HAWRAT	Highways Agency Water Risk Assessment Tool
HRDB	Highway Runoff Database
IDF (curves)	Intensity-duration-frequency (curves)
IF	Impervious fraction
MC	Month constant
MHI	Maximum hourly intensity
MLR	Multiple linear regression
P_{annual}	Annual average rainfall
PAH	Polycyclic aromatic hydrocarbon
PC	Pollutant constant
PROPER	Project Road Runoff Pollution Management and Mitigation of Environmental Risks
R^2	Coefficient of determination
RMSE	Root mean square error
S	Average slope
SELDM	Stochastic Empirical Loading and Dilution Model
SMC	Site mean concentration
T_c	Concentration time
TER	Total event rainfall
TSS	Total suspended solids
USA	United States of America

1 Introduction

1.1 Road runoff pollution

In the context of the growing environmental concern worldwide, the quality of the water bodies is a major issue. Some management strategies to control nonpoint and point source pollution have been applied. One source of nonpoint pollution of these water bodies comes from road runoff, which may have much lower quality than the effluent of some wastewater treatment plants (Ringler, 2007). Thus, there is a need to study and provide better tools to support decision makers on the management of the quality of these water bodies. One of the most worrisome concerns at the national level is the lack of any specific legislation to evaluate this type of runoff. The Portuguese Decree-Law n.º 236/98[1], from 01 of August, which establishes quality standards, criteria and objectives for the purpose of protecting the aquatic environment and improving water quality in relation to its main uses is currently being used as legal framework to support the study of road runoff. It is important to notice that this Decree-Law is only used as a reference to the researchers, due to the fact that road runoff has very different characteristics than the rejected water from the wastewater treatment plants, for several reasons, such as: (i) the legislation is applicable only for punctual and not for diffuse pollution, which is the case of road runoff pollution and (ii) on road runoff, the seasonality is much more clear than in the waters from the wastewater treatment plants.

In response to the European environmental concern, the Water Framework Directive (OJEC, 2000) has emerged, which requires a good understanding of the impacts of pollution sources and also the control of the most relevant to the receiving water bodies. In the case of roads, Barbosa *et al*. (2011) argues that it is important that the assessment of concentrations and pollutant loads take into account the characteristics not only of the road, but also of the climate. The prediction of the quality of a road runoff is a rather challenging issue due to its stochastic and diffuse nature. Winkler (2005) states that, even more complicated is the ability to assess the impact of pollutants on the receptor medium due to the need to analyse the case over a large time scale (*e.g.* due to persistent substances).

In this dissertation, previously collected data of road runoff of six European countries were gathered and compared to the predictions of four models. In order to provide decision makers with the most reliable tools, an assessment of these models was performed. Moreover, a regression model intended to predict total suspended solids (TSS), copper, zinc, lead and cadmium site mean concentrations (SMC) was also developed using the data from six European countries.

1.2 Scope and objectives

The current work is part of an European research project, funded by the *Conference of European Directors of the Roads*, entitled *Project Road Runoff Pollution Management and Mitigation of Environmental Risks* (PROPER). It aims at reviewing and generating knowledge that can be used at European level. Several studies have been developed in this area in view of a greater environmental

---

[1] In this dissertation, the norms of the Portuguese Decree-Law n.º 236/98 from 01 August considered were the Emission limits values of wastewater discharge, present in the annex XVIII of the same Decree-Law.

concern, having in this case a preponderance over water. The dissertation is included in the Work package 1 (*cf*. Figure 1.1).

The pollutants generated through the traffic and road construction and maintenance can be automatically deposited in the soil, or emitted into the air and subsequently, some of them, deposited due to gravitational force or precipitation reaching the closest surface water bodies, as indicated in Figure 1.1. Although the sources of pollutants in these infrastructures are well defined, literature indicates that the prediction of pollutant loads and concentrations is uncertain. This uncertainty is due to the several variables at stake, for instance, the type of pavement of the road, the antecedent climatic conditions and the intensity, frequency and magnitude of rainfall events. These must be viewed as a stochastic phenomenon as it is impossible or not realistic to determine the exact process boundary conditions (Fernandes and Barbosa, 2018).

Tools that apply to the understanding of pollutant sources, their mobilisation, transport to the receiving environment and groundwater, should be seen not in an exact context, but through a statistical or risk assessment (Fernandes and Barbosa, 2018).

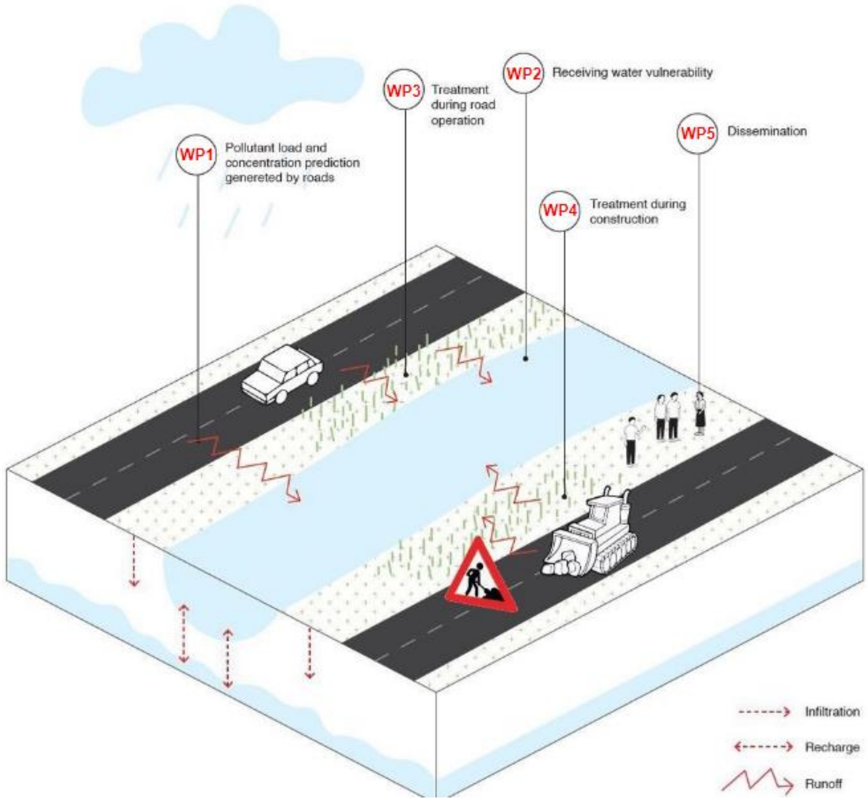


Figure 1.1 – Representation of road runoff and probable ways of reaching surface water bodies (source: http://proper-cedr.eu/index.html)

The current work has the following main objectives:

(i) Characterisation of the road runoff in and European context;

(ii) Collection and analysis of available monitored data;

(iii) The assessment of road runoff predicting tools (HAWRAT - Highways Agency Water Risk Assessment Tool; SELDM - Stochastic Empirical Loading and Dilution Model; PREQUALE and Kayhanian's multiple linear regression method).

(iv) Development of a new SMC prediction model.

1.3 Dissertation structure

The dissertation is divided into six distinct chapters, the contents of which are summarised below. The present chapter presents the introduction and the objectives of the dissertation. In the second chapter, a review of the worldwide existing literature is presented, focusing essentially on the European references. This section corresponds to a generic characterisation of road runoff pollution, a description of the pollutants and corresponding sources and the distinction between acute and cumulative impacts. Moreover, specific cases like highways maintenance and accidental spillages, concentrations and loads calculations and a brief view of road runoff model types are presented.

The third chapter comprises the monitoring data collection for each country, its comparison with the legal regulated limits and the description of the predicting models that were assessed in the current work.

The fourth chapter concerns the assessment of the predicting tools. After a sensitivity test of a specific model, the methodology followed for the assessment is presented. Issues like the input data and the easiness of application are presented. Finally, a critical review is presented for each of the models, comparing their predictions with the monitoring data

The fifth chapter concerns the development of a new model. This model is the only model studied in this work that was calibrated with European data from more than one country.

In the final chapter, the discussion of results and conclusions are presented.

2 Literature review

2.1 Road runoff pollution

2.1.1 Generic characterization of road runoff pollution

A shift of the main concern about water management from quantity to quality and quantity has been noticed. In addition to this concern, there was an attempt to ensure the integrated management of the resource in a perspective of strong sustainability, considering the technical, economic, social and ecological aspects (Coelho, 2009).

Several studies were developed to manage and preserve the water resources. The main difference that can be pointed out in relation to the possible inputs of pollutants into the receiving bodies concerns the distinction between point and nonpoint source or diffuse pollution. The first refers to a direct and easily identifiable input (*e.g*. a pipe) of a polluted effluent while nonpoint source pollution corresponds to an effluent input from various origins like superficial runoff, atmospherically deposition, precipitation or infiltration, which origin is hard or almost impossible to identify, as stated by Loague and Corwin (2005).

Road runoff is often seen as an effluent with well-defined characteristics. Still, it covers a complex matrix of pollutants mainly dependent on various factors such as traffic or the characteristics of the site where they are generated. Barbosa *et al.* (2011) highlights that the potential impact of these pollutants must be studied taking into account both pollutant and the receiving environment characteristics. The Water Research Council points out, in a report of 2002 (as cited in Higgins, 2006), that the base pollutant matrix of a road runoff water is composed of solids, metals, hydrocarbons and inorganic salts, as indicated in Table 2.1. All these pollutants, depending on their quantity and state, can have a detrimental impact on receiving surface and underground water bodies (Barret *et al*., 1995 in Higgins, 2006*)*. The main anthropogenic sources that lead to the above-mentioned pollutant matrix are not only the circulation of vehicles on the highways and their maintenance as can be easily verified in CIRIA report of 1994 (in Higgins, 2006), but also road signs as indicated by Barbosa *et al.* (2011).

Road runoff is recognised as a nonpoint source pollution. Thus, there is a responsibility for the management operators and the national authorities to ensure that these discharges comply with their respective national legislation, which has been reinforced by the European Union Water Framework Directive (Barbosa *et al*., 2011). Since its implementation, there has been a greater need to define the source of pollutants affecting the receiving environment and the need for nonpoint source pollution management (OJEC, 2000 in Higgins, 2006). Therefore, improvements on water treatment strategies have been continuously developed.

Higgins (2006) pointed out the five main categories of factors affecting contaminant concentrations namely: (i) Traffic volume and characteristics; (ii) Precipitations characteristics and pattern; (iii) Surrounding land use; (iv) Pavement structure and material used in construction; (v) Pollutant characteristics.

Regarding the effects of the traffic volume in the road runoff pollution, at least three different ways of measuring traffic volume can be identified (Irish *et al*., 1995): (i) Vehicles travelling during the storm (VDS); (ii) Vehicles travelling in the antecedent dry period (VADP); (iii) Annual average daily traffic (AADT).

The classification of traffic volume could be made in several ways. While many road agencies use AADT to determine whether or not a highway needs to have a treatment system for their runoff, there are several authors who have found no relationship between this indicator and the load and concentration of solid pollutants, heavy metals, oils and lubricants (Higgins, 2006). Irish *et al*. (1995) suggests that the number of vehicles traveling during a storm may be a significant factor in determining pollutant loads, since they are in direct contact with precipitation during a high rainfall event.

Regarding the precipitation characteristics, three main indicators are commonly found in literature to assess its influence in road runoff pollution, namely: (i) Antecedent dry period (ADP); (ii) Rainfall intensity; (iii) Runoff volume. ADP is defined as the period of time with no runoff (days or hours) preceding a storm event (Irish *et al*., 1995). An early research from Howell (1978) (in Irish *et al.,* 1995) suggests that the preceding dry period was significant to the build-up of solids on the highway and the corresponding pollutant loads in the runoff. The rainfall intensity is a key factor in relation to the pollutant loadings because the rain is the main driving force in which contaminants are removed from the air, vehicles and the highway surface (UK Transport Research Laboratory, 2002).

The characteristics of precipitation are the most important for the occurrence of the so-called "First-Flush" effect. This phenomenon occurs when a precipitation event is preceded by an ADP of several days. During the beginning of the rain event, road runoff water pollution is typically more pollutant concentrated compared to the rest of the storm. The first-flush phenomenon is affected by certain parameters like the size of the watershed, rainfall intensity, impermeable area and the antecedent dry weather period. The concentration peak varies for each pollutant during the same rainfall event or in the same watershed during different rainfall events (Wanielista and Yousef, 1993 in Yannopoulos *et al*., 2013). The occurrence of a first-flush effect in a road runoff event is exemplified in Figure 2.1.

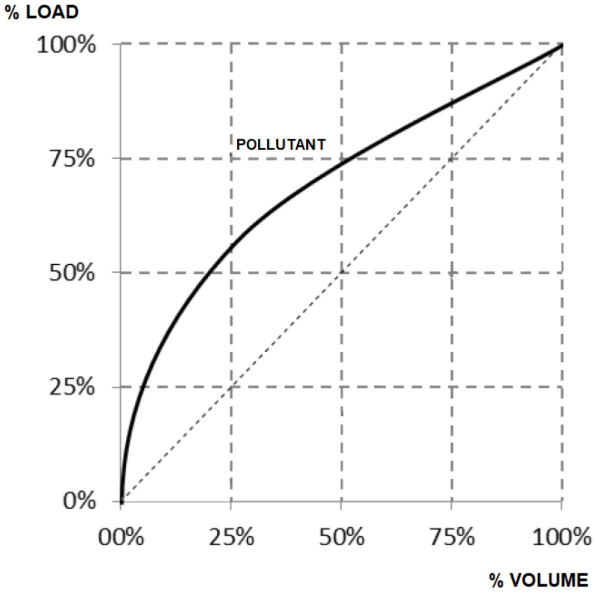


Figure 2.1 – Example of first-flush effect (Adapted from: Antunes, 2014)

2.1.2 Pollutants and sources

Road traffic, weather conditions and the highways maintenance are responsible for the transport of the road runoff to the receiving environment (Piguet, 2007 and Kobriger and Geinepolos, 1984). The main pollutants comprise solids, heavy metals, inorganic salts and hydrocarbons. A list of pollutants and their sources are listed in Table 2.1.

Table 2.1 – Main pollutants and associated sources (Higgins, 2006)

Pollutant	Specific Contaminant	Source
Solids	Carbon	Exhaust, Oil
	Organic Solids	Oil, Exhaust
	Rubber	Tyres
	Plastic	Vehicles
	Grit	Deicing salts, Road structure
	Asbestos	Brakes, Clutches
	Rust	Vehicles
	Metal Filings	Vehicles
Metals	Arsenic	Fuel
	Barium	Paints, Rubber
	Cadmium	Tyres, Oils, Galvanised metals
	Calcium	Oils, Deicing salts
	Chromium	Metal plating, Bearings, Brushings
	Copper	Paints
	Iron	Tyres, Brakes, Oils, Bearings
	Lead	Corrosion
	Magnesium	Fuel, Tyres, Brake linings, Bearings
	Manganese	Cast metal
	Nickel	Tyres, Brakes, Oils, Bearings
	Zinc	Fuel, Paints, Tyres, Lubricants, Corrosion, Brakes
Hydrocarbons	Aliphatic Hydrocarbons	Lubricant, Fuel, Anti-freeze
	Poly Aromatic	Fuel, Lubricants
	Hydrocarbon	Lubricants, Fuel, Anti-freeze
	Phenols	Combustion products
	Carbonyl Compounds	Road surface
	Bitumen	Road surface
	Asphalt	Spillages
	Solvents	Fuel combustion
	Polychlorinated biphenyl (PCB)	Fuel combustion
	Methyl tert-butyl ether (MTBE)	Fuel combustion
Inorganic Salts	Nitrates	Lubricating oil
	Chlorides	Deicing salts
	Phosphates	Lubricating oil
	Herbicides	Road verges (maintenance activities)

As not all the pollutants from runoff presented in Table 2.1 are regularly monitored, Kayhanian *et al*. (2012) suggested a selection of the most important parameters to be monitored to evaluate the road runoff (*cf.* Table 2.2).

Table 2.2 – Road runoff components division (Kayhanian *et al.,* 2012)

Runoff Components	
Conventional and aggregate water quality parameter	TSS; Total dissolved solids; Dissolved organic carbon; Total organic carbon; Chemical oxygen demand (COD); Biochemical oxygen demand; Oil and grease; Hardness as $CaCO_3$; Temperature; pH
Metal constituents	Most frequently: Cadmium; Chromium; Copper; Lead; Nickel; Zinc Less frequently: Aluminium; Arsenic; Iron
Nutrient constituents	*Nitrates; Ammonium; Total Kjeldhal nitrogen; Total nitrogen; Total phosphorus
Infrequently measured water quality parameters	Fecal indicator bacteria; Toxicity; Polycyclic aromatic hydrocarbons (PAHs); Herbicides; Pesticides

*Kayhanian *et al*. (2012) also points out that the presence of phosphorus and nitrogen as pollutants in the monitoring of runoff water is due not only to pollutant sources related to road traffic, but also due to external factors.

The mentioned pollutants are not only caused by road traffic. They may come from several sources, both anthropogenic and natural. Some are transported long distances by the wind, being deposited later in the most varied places as stated by Fritzer (*in* Winkler*, 2005*). According to the same source, the most relevant related pollution sources are: the abrasion of road surfaces; the abrasion of tires; drip loss; combustion emission; the abrasion of brake pads and clutch plates.

After considering road traffic and emitted pollutants into the atmosphere as the first and second source of road pollution, Barbosa *et al.* (2011) pointed out the maintenance and construction activities as a third source of pollutants. As far as construction is concerned, the largest pollutants are related to solids and accidental cases, such as situations with fuels, oils and lubricants. Regarding the road maintenance, the main sources of pollutants are the de-icing salts (chlorides) used in some parts of Europe, where snow and ice abound during the colder periods of the year, as well as herbicides, which in high concentrations lead them to be a persistent pollutant in the ecosystem (Mudge and Ellis, 2001 *in* Higgins, 2006).

2.1.3 Receiving waters impacts

The potential impacts of each pollutant in the receiving water are presented in Table 2.3.

Table 2.3 – Main impacts per type of pollutants

Pollutant	Impacts
Solids	Reduce light transmission which limits photosynthesis and diminishes aquatic food supply (Goldman, 1986 and Barret *et al.,* 1995 in Winkler, 2005); Lead to an elevated level of insoluble substances with negative impacts on fish eggs and larvae trough clogging of the pores between the substrate of the riverbed (Winkler, 2005); Clog fish gills and harm their respiration and the respiration of other aquatic animals (Hill, 2010).
Metals	Can be toxic because metals undergo bioconcentration (Salomon, 2008). The toxicity associated may reduce diversity and abundance of the sensitive aquatic biota and replace them with pollution tolerant species (Hvitved-Jacobsen and Yousef, 1991); Copper, cadmium and zinc could be toxic even in low concentrations (Scheffer and Schachtschabel, 2002 and Hahn, 2004 in Winkler, 2005).
Hydrocarbons	Several PAHs are toxic, mutagenic/carcinogenic. This type of pollutants is highly lipid soluble and thus easily absorbed by human bodies (Abdel-Shafy and Mansour, 2015). Methyl-Tertiary-Butyl-Ether (MTBE) is toxic to several freshwater organisms (Werner *et al.,* 2001).
Inorganic Salts	Like fertilizers and herbicides, used in the maintenance of road shoulders, essentially on the roadside, lead to an increase in phosphorus and nitrogen in the runoff matrix, which contributes to the eutrophication of the receiving environment (Hvitved-Jacobsen and Yousef,1991).

2.1.4 Acute and cumulative impacts

Depending on the pollutant type, concentration, rate of assimilation of organisms, and on its form (dissolved and particulate), the impacts created in the water environment may be acute or cumulative.

Acute effects are associated with accidental spills and/or organic or metallic pollutants entering the composition of road runoff. Other examples of acute effects are the presence of copper in its soluble form, soluble short-chain organic pollutants (*e.g*. herbicides) and runoff of suspended solids (in case of road maintenance campaigns, or after a long period without occurrence of precipitation) as stated by Barbosa *et al*. (2011). Hvitved-Jacobsen and Yousef (1991) defined that the impacts that cause this kind of effects are characterised by short duration events and that the impact declines after the discharge is over; even if the events last for few days it is still considered an acute impact.

Cumulative effects are associated with less soluble metals (although their solubility depends on particle characteristics, water hardness, iron and aluminium oxides content and relative concentration), thus being related to a toxicity that develops due to accumulation pollutants in the tissues of organisms. The most persistent hydrocarbons (as PAHs) are usually considerate as the particulate fraction of the pollutants. The physical accumulation of sediments such as silt and clay can change the ecosystem by covering surfaces and choking flora and fauna. Chronic effects may occur when these sediments are contaminated with PAHs or metals (Barbosa *et al*., 2011). Besides that, Hvitved-Jacobsen and Yousef

(1991) refers that other type of pollutants that may lead to cumulative impacts are nutrients namely to the eutrophication of low hydrodynamic media such as reservoirs.

2.1.5 Specific cases

There are two main types of specific cases in highway runoff pollution, which are not due to the continuous vehicles traffic: (i) Highway maintenance; (ii) Accidental spillage.

The most varied pollutants are associated with the maintenance activities of a highway, as indicated in Table 2.1. Pollutants like herbicides and nutrients are found in highway runoff essentially as a result of highway maintenance activities and adjacent land-use contributions as stated in Maestri *et al*. (1988). Another example is the high sediment movement during maintenance works as well as leaks of fuels, oils and grease, hydraulic fluids, among others (Barbosa *et al*., 2011). On highly trafficked highways, where there are already systems for the treatment of runoff water, it is necessary to be concerned with the construction waste and maintenance of treatment systems (for example sedimentation sludge removal) (Barbosa *et al*., 2011).

The risk of a leak on a road is very likely due to events such as the leakage of oils and fuels in a car or the leakage of products transported in heavy goods vehicles. Barbosa *et al*. (2011) states that when a spill hits a water receiving body, it normally causes acute pollution. However, sometimes the product resulting from the spill will infiltrate and pollute the groundwater.

2.1.6 Concentrations

In order to evaluate and study road runoffs, it is necessary to define some concepts whose equations units are presented in dimensional analysis. Event mean concentration (EMC) is defined as the pollutant concentration of a composite of multiple samples collected during the course of a storm (Thornburg and Lowe, 2009), as represented in the equation 2.1 (*e.g.* Antunes, 2014).

$$\mathrm{EMC}=\frac{\sum_{j=1}^{n} C_j \times V_j}{\sum_{j=1}^{n} V_j} \tag{2.1}$$

EMC – Event mean concentration (ML^{-3})
j – Number of time intervals analysed by each event
V_j – Volume in each time interval j (L^3)
C_j – concentration of the pollutant in V_j volume (ML^{-3})

This dissertation aims to calculate the SMC *i.e*. the average (equation 2.2) or the median of the monitored EMC of each site. When the number of monitored events is very low, it is usual to use the average (Barbosa *et al*., 2011).

$$SMC= \frac{\sum_{k=1}^{N} EMC_k}{N} \tag{2.2}$$

SMC – Site mean concentration (ML^{-3})

$\sum_{K=1}^{N} EMC_k$ – Event mean concentration for a storm k (ML^{-3})

N – Total number of storms sampled at a given catchment

2.2 Tools to predict road runoff

Sitterson *et al.* (2017) presented an overview of runoff model types. The authors divide the models in three mains categories: (i) conceptual; (ii) Physical and (iii) Empirical.

Conceptual models connect simplified hydrology components and are based on simplified hydrological processes which provide a conceptual look regarding the catchment area as stated by Vaze in 2012 (in Sitterson *et al.,* (2017).

Physical models are based on the understanding of the physics related to the hydrological processes. Physically based equations govern the model to represent multiple parts of real hydrologic responses in the catchment (Vaze, 2012 in Sitterson *et al*., 2017).

Empirical models involve mathematical equations that are derived from observations of the inputs and outputs. In these models, runoff modelling is based in temporal data series (Granata *et al*., 2016).

Some examples of empirical models are regression analysis, artificial neural networks (ANN) and Monte Carlo methods. Regression analysis could be seen as a set of statistical processes to estimate the relationships between variables. This method allows to understand how the changes in the independent variable influences the dependent variable (Ramana, 2014). Monte Carlo methods simulate random values which give an approximate solution of a mathematical or physical problem (Sobol 1974; Rubenstein, 1981 in Karlovits, 2010).

3 Data and Methods

3.1 Data collection

The assessment of the models was made considering the comparison between the prediction and monitored data. The former is related to SMC of 20 roads in Europe. These data were collected from direct contacts to the road and research institutes dealing with road runoff. A summary of the main characteristics of the monitored roads is presented in Table 3.1.

Table 3.1 – Road characteristics

Country	**Highway**	**Code**	**Drainage Area (DA)** (m^2)	**Impervious fraction (IF)** (0-1)	**Annual precipitation (P_{annual})*** (mm)	**Annual average daily traffic (AADT)** (no. vehicles)
Portugal	A 1	P1	22 800	0,412	645,95	27 746
	A 2	P2	1 287	1	527,98	16 344
	A 6	P3	5 580	1	744,43	2 918
	A 22	P4	15 422	0,85	518,33	24 000
	A 25	P5	287	1	1 013,76	15 673
	IP 6	P6	7 280	1	708,61	6 539
Netherlands	A 27 - pervious	N1	48 590	0,5	776,00	63 000
	A 27 - Impervious	N2	30 510	1	776,00	63 000
Norway	E 6	N3	22 000	1	834,42	42 000
France	A 11 - pervious	F1	3 200	1	786,00	24 103
	A 11 - impervious	F2	3 200	0,5	786,00	24 103
Ireland	M 7 - Kildare	I1	14 184	1	731,00	27 500
	M 7 - Monasterevin	I2	11 368	1	731,00	27 500
	M 7 - Portlaoise	I3	9 600	1	731,00	27 500
England	M 4 - Brinkworth	E1	8 755	1	745,20	70 000
	M 4 - River Ray	E2	4 348	1	745,20	35 000
	M 40	E3	58 680	1	614,80	78 000
	A 417	E4	20 232	1	843,40	24 000
	A 34 - Gallos Brook	E5	2 760	1	659,70	64 000
	A 34 - River Enborne	E6	19 425	0,5	635,40	36 000

*P_{annual} information is available at: https://snirh.apambiente.pt/; https://www.climatedata.eu; https://fr.climate-data.org; https://weather-and-climate.com; https://www.metoffice.gov.uk

In Figure 3.1 the location of the monitored sites in an annual average precipitation map is presented.

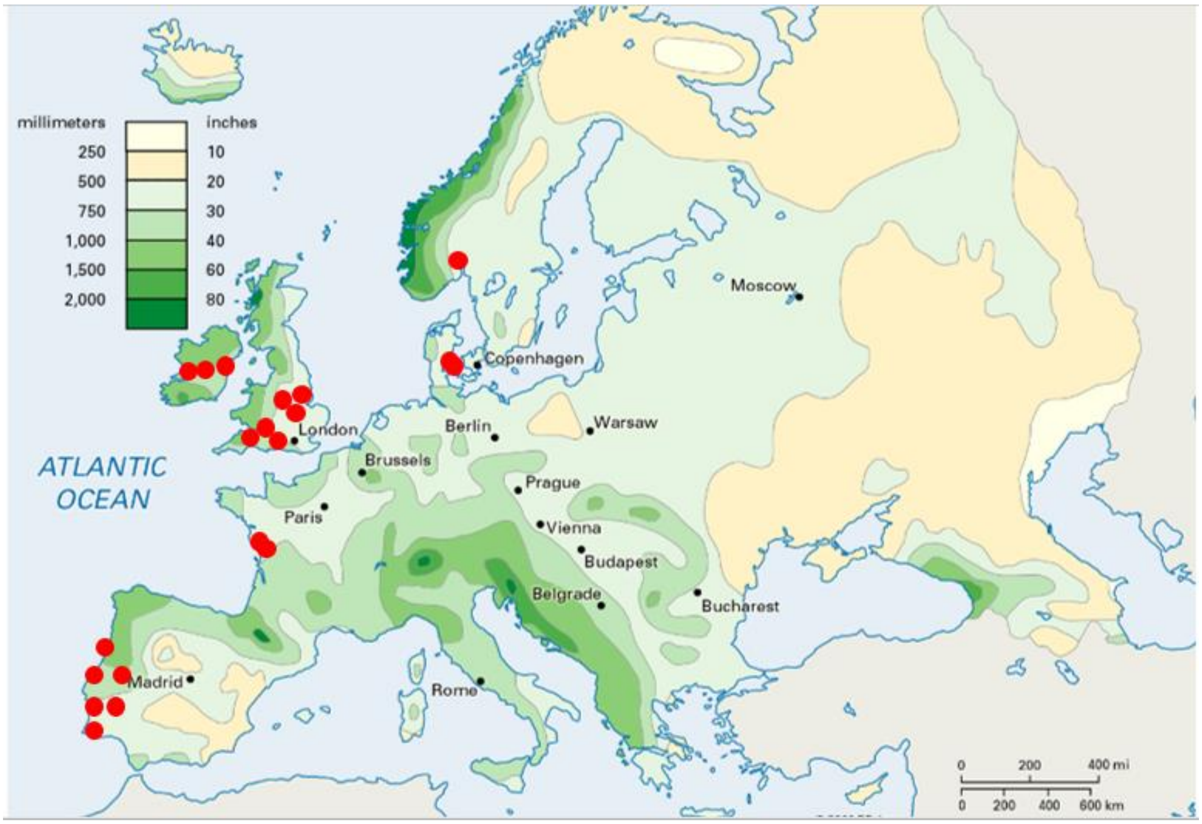


Figure 3.1 – Europe precipitation map with the roads under study[2]. Each dot corresponds to one road

As previously referred, in order to check which of the tools under study is better adapted to the collected data, the results predicted for each tool were compared to the monitored data. The monitored data is presented in Appendix 1. In order to treat the monitored data, for each site and each pollutant, the EMC values were averaged to calculate the mean SMC. These data were compared with the wastewater emission limit defined by the Portuguese Decree-Law n.º 236/98, from 01 of August. This analysis is presented in Table 3.2, where it was verified that only TSS are above the limit (60 mg/L). The precipitation hourly data series was collected or made available by the project partners.

Table 3.2 – SMC of each site

Highways	**TSS** (mg/L)	**Cu** (µg/L)	**Zn** (µg/L)	**Pb** (µg/L)	**Cd** (µg/L)
P1	22,96	19,24	124,07	4,38	0,09
P2	2,50	11,13	69,00	2,10	
P3	19,65	8,10	345,83	1,83	
P4	52,44	24,44		23,33	
P5	57,93	86,86	139,69	28,65	
P6	207,08	31,45	73,17	7,67	1,09
N1		114,71	500,88	29,88	1,60

---

[2] https://eldoradoweather.com/forecast/climate/climate-maps/europe-annual-precip-map.html

Highways	**TSS** (mg/L)	**Cu** (µg/L)	**Zn** (µg/L)	**Pb** (µg/L)	**Cd** (µg/L)
N2		29,14	118,86	14,43	1,00
N3	227,61	84,09	224,87	14,70	0,21
F1	71,38	45,51	356,08	57,93	1,03
F2	10,89	27,37	160,05	11,64	0,43
I1	856,44	123,29	666,67	139,38	8,70
I2	155,74	48,95	198,25	68,91	4,86
I3	49,52	24,70	82,00	76,90	8,61
E1	88,60	30,00	100,70		
E2	310,87	54,61	221,50	68,98	1,77
E3	50,88	42,65	149,31	15,16	0,43
E4	64,76	23,99	52,60	4,38	0,21
E5	101,13	67,92	219,73	50,45	0,62
E6	82,70	32,46	29,01	16,57	0,25
Decree-Law n.º 236/98 emission limit	60,00	1 000,00		1 000,00	200,00

3.2 Description of the models

3.2.1 PREQUALE

In the scope of the research project – G -Terra – funded by the Portuguese Foundation for Science and Technology and coordinated by the National Laboratory for Civil Engineering, the road runoff from several roads was monitored between 2002 and 2006 (Barbosa *et al.*, 2011). Using the data of six roads, the first version of the tool PREQUALE which stands for *Previsão da Qualidade das Águas de Escorrências* (Road Runoff Quality Prediction) was developed. This tool aims at directly predict SMC. It is based on the following principles: (i) input data easily available for designers; (ii) easiness of calculation; (iii) clear and transparent model and (iv) reliable results at national level.

The applicability of the tool is rather simple as it is based on a multiparametric equation (equation 3.1) with the following input variables:

(i) Drainage area (DA in km^2) – area which contributes with runoff to the discharge point during a rainfall event;
(ii) Impervious fraction (IF in %) – the percentage of the total drainage area which is impervious;
(iii) Average annual rainfall volume with the same duration as the basin time of concentration (AR in mm) – further details on its calculation will be provided below;
(iv) Annual average precipitation (P_{annual} in mm).

The multiparametric equation takes the following form:

$$SMC = a_i \left(DA^{\beta_1} \times IF^{\beta_2} \times AR^{\beta_3} \times P_{annual}{}^{\beta_4}\right) \tag{3.1}$$

where SMC is the estimated site mean concentration of each pollutant and a_i, β_1, β_2, β_3 and β_4 are the corresponding regression coefficients.

The AR was calculated in order to denote a representative rainfall event of the region. It was assumed that this event is the average precipitation with a duration equal to the time of concentration of the basin and with a return period of two years. To calculate this variable, it is necessary to use auxiliary calculations: firstly, the time of concentration of the drainage basin has to be determined (*e.g.* equation 3.2, in Lencastre and Franco, 1984).

$$t_c = 0{,}0663 \times \frac{DL^{1{,}155}}{\Delta h^{0{,}385}} \tag{3.2}$$

t_c – Concentration time (hours)

DL – "Main river" length (Km) - (in this case is the maximum length of the road in the drainage basin)

Δh – Slope (m) - heights difference between the ends of the road

Secondly, the volume is calculated using intensity-duration-frequency (IDF) curves with a return period of 2 years. For Portugal, the report Brandão *et al*. (2001) was used.

The current version of PREQUALE allows the prediction of SMC for TSS, chemical oxygen demand (COD), Fe, Zn and Cu. This tool was validated for the situations in which the parameters' values were between the values presented in Table 3.3.

Table 3.3 – Intervals for which PREQUALE had been validated (Adapted from: Barbosa *et al*., 2011)

Parameter	Lower limit	Upper limit
AR (mm)	6,0	7,5
DA (Km^2)	$2{,}5\times10^{-4}$	$6{,}5\times10^{-2}$
IF (%)	40	100
P_{annual} (mm)	560	1 200

In Table 3.4 the road characteristics for each road used to calibrate PREQUALE are presented while the regression and correlation coefficients that resulted from the adjusted multiparametric equation of the roads SMC are presented in Table 3.5.

Table 3.4 – PREQUALE roads (Adapted from: Barbosa *et al*., 2011)

Road	AR (mm)	DA (km^2)	IF (%)	P_{annual} (mm)	Observations
A1	7,5	$6{,}46\times10^{-2}$	41,2	1 157,0	Runoff drains to the treatment system
A3 Santo Tirso	6,8	$2{,}00\times10^{-3}$	100,0	782,0	Descending section
A3 Ponte de Lima	6,1	$2{,}45\times10^{-3}$	100,0	1 537,4	Ascending section
A6	6,5	$5{,}58\times10^{-3}$	100,0	761,0	Runoff drains to the treatment system
A25	6,0	$2{,}50\times10^{-4}$	100,0	929,0	Near Aveiro lagoon
IP6	6,0	$7{,}28\times10^{-3}$	100,0	902,0	Runoff drains to the treatment system

Table 3.5 – PREQUALE regression and correlation coefficients (Adapted from: Barbosa *et al*., 2011)

Parameter	a_i	β_1 (DA)	β_2 (IF)	β_3 (AR)	β_4 (P_{annual})	Correlation Coefficient
TSS (mg/L)	$1{,}22\times10^{44}$	0,257	-5,085	-28,797	-2,945	0,9696
COD (mg/L)	$1{,}91\times10^{25}$	0,1644	-3,165	-16,914	-1,064	1,0000
Fe (mg/L)	$9{,}20\times10^{44}$	-0,1491	-6,546	-28,229	-3,371	1,0000
Zn (mg/L)	$1{,}15\times10^{05}$	-0,135	-1,08	-0,323	-1,296	0,8843
Cu (mg/L)	$3{,}08\times10^{01}$	0,036	-0,705	0,396	-0,702	0,9989

3.2.2 Highways Agency Water Risk Assessment Tool (HAWRAT)

HAWRAT was developed by Highways Agency from the United Kingdom as a standalone application aiming at helping highway designers decide if road runoff pollution mitigation measures are needed.

This tool allows the prediction of (i) soluble pollutants and (ii) sediment related, expressed as EMC for total copper, zinc, cadmium, pyrene, fluoranthene, anthracene, phenanthrene and total PAH. As the model predicts EMC, it is necessary to calculate several EMC (in a time frame) in order to predict the SMC.

Besides the prediction of runoff quality, HAWRAT also incorporates models to predict the impact of the runoff on receiving rivers and streams, as shown in Figure 3.2. HAWRAT comprises three steps: Step 1 concerns road runoff pollution prediction, Step 2 is related to the impacts in the receiving water bodies and Step 3 deals with the selection of mitigation measures. In the scope of the present work, the results of steps two and three were not analysed.

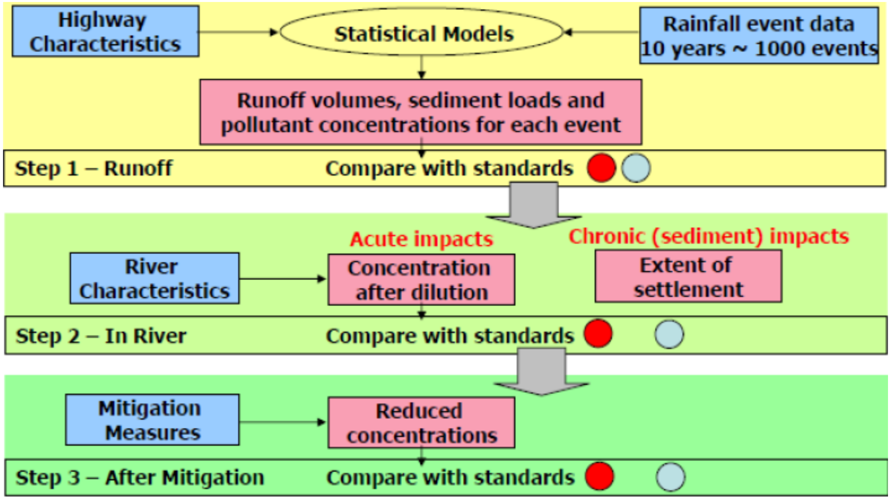


Figure 3.2 – HAWRAT methodological scheme (Jotte *et al*., 2017)

HAWRAT should not be used in certain cases, such as: (i) Urban Highways; (ii) Highways with traffic densities outside the range of 11 000 – 159 000 vehicles/day (it can be used for highways with traffic density less than 11 000 vehicles/day but the result may be overestimated) and (iii) Highways discharging to receiving watercourse that are tidal and/or saline (Highways Agency, 2009). The agency also emphasises that the tool can be applied in Wales, Scotland and Northern Ireland, although the basic data was generated in England, and recalls its limited ability to assess the impact on streams where the flow is intermittent or seasonal.

As described by the Highways Agency (2009), in order to use the graphical interface, HAWRAT uses an auxiliary software that stochastically generates hourly rainfall series of the United Kingdom and calculates a main part of the mandatory inputs of the tool.

However, the pollutants that were intended to be studied in this work were not available in the automatic tool. Instead, the equation that was the basis of HAWRAT was used to predict the runoff pollution. This equation (equation 3.3) is a multiple linear regression resulting from a study (Crabtree *et al*. (2008) and Dempsey and Song (2008)). Equation 3.3 allows the user to predict TSS, total copper, total zinc and total cadmium and has the following input variables:

(i) Pollutant constant (PC) - Fixed to each pollutant;
(ii) Climate region constant (CRC) – Also fixed to each pollutant;
(iii) Annual average daily traffic constant (AADTC) – Dependent of the number of cars per day;
(iv) Month constant (MC) – Fixed and based on the month that the precipitation event occurs;
(v) Maximum hourly precipitation (MHI in mm/h) – The highest value of hourly precipitation registered in a precipitation event;
(vi) Antecedent dry period (ADP in hours) – Number of hours without precipitation since the last precipitation event.

$$\log_{10} \mathrm{EMC} = \mathrm{PC} + \mathrm{CRC} + \mathrm{AADTC} + \mathrm{MC} + \gamma_1 \times \mathrm{MHI} + \gamma_2 \times \mathrm{ADP} \tag{3.3}$$

Where log_{10}EMC is the event mean concentration of the studied pollutant and γ_1 and γ_2 are the regression coefficients presented in Table 3.6.

CRC is only defined for the region where HAWRAT is applicable (Figure 3.3). In this way, it was defined that the red lines that separate each climatic region will continue indefinitely, so the countries northwest of England will have an "cold/wet " climate, countries to the northeast will have a " cold/dry" climate, countries to the southwest will have a " warm/dry" climate and countries to the southeast will have a "warm/wet" climate.

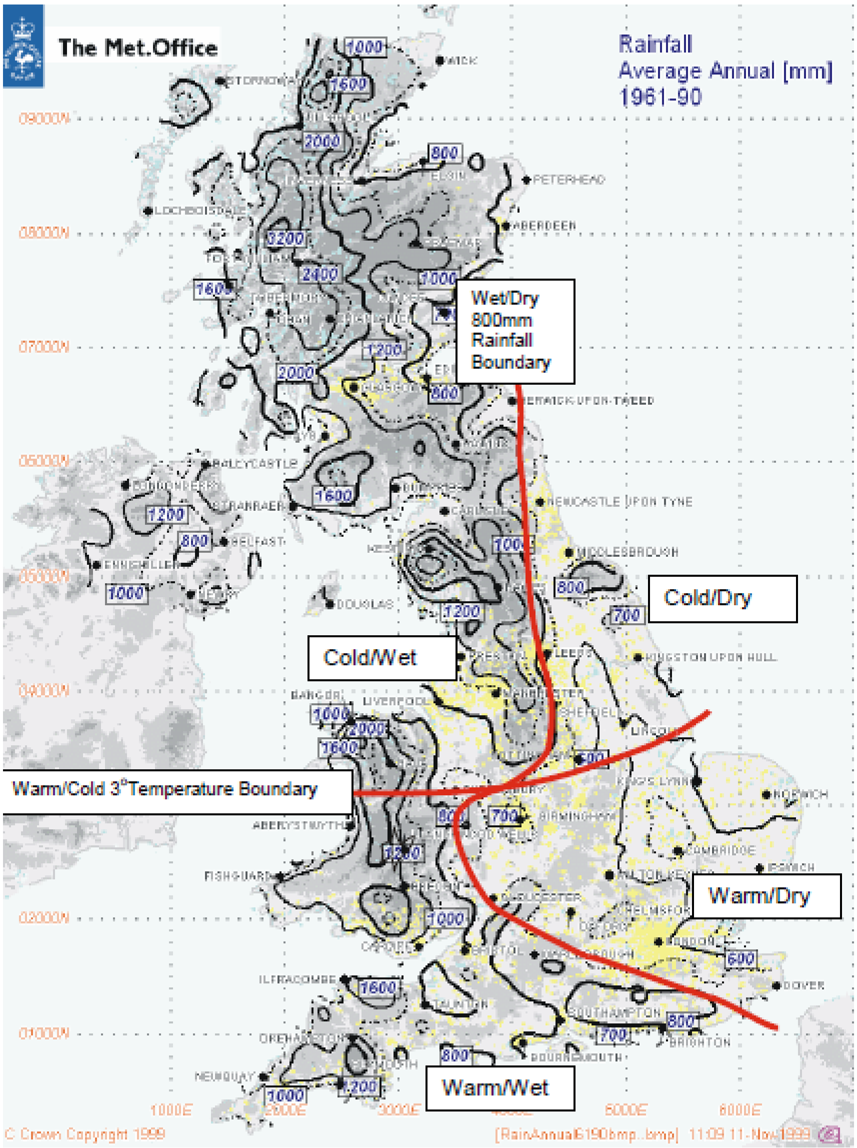


Figure 3.3 – Representative map of the limits/areas used in HAWRAT (Crabtree *et al.,* 2008)

The constants needed for the HAWRAT equation for each combination of region, traffic, month and pollutant are presented in Table 3.6.

Table 3.6 – Constants table in order to predict concentrations trough HAWRAT (Adapted from: Dempsey and Song, 2008)

	Inputs	**EMC constants**			
		Total Copper	**Total Zinc**	**Total Cadmium**	**TSS**
Site	Constant	1,394	1,91	-0,832	2,1
	Colder/Dry	0	0	0	0
	Colder/Wet	0,042	0	0	-0,217
	Warm/Dry	0,144	0	0	-0,248
	Warm/Wet	0,089	0	0	-0,163

	Inputs	EMC constants			
		Total Copper	Total Zinc	Total Cadmium	TSS
Traffic	AADT<50000	0	0	0	0
	50000=<AADT<100000	0,018	0,045	0,093	0
	AADT>=100000	0,512	0,502	0,379	0
Months	1	0,402	0,662	0,773	0,535
	2	0,568	0,699	0,565	0,443
	3	0,526	0,704	0,625	0,324
	4	0,427	0,504	0,374	0,193
	5	0,559	0,716	0,579	0,288
	6	0,425	0,32	0,241	0,283
	7	0,258	0,27	0,064	-0,148
	8	-0,064	-0,154	-0,216	-0,108
	9	0,065	-0,098	-0,067	-0,101
	10	0	0	0	0
	11	-0,028	0,068	0,05	0,022
	12	0,085	0,231	0,181	0,491
Extra	MHI	0	0,022	0	0,065
	ADP	0	0	0	0

3.2.3 Kayhanian's multiple linear regression method

Kayhanian *et al*. (2006) proposed a multiple linear regression (MLR) to predict EMC. This regression was undertaken with the following specific objectives: (i) Provide a statistically summary of highway runoff quality in California, United States of America (USA); (ii) Discuss the impact of selected independent event and site characteristics parameters on highway runoff constituent EMC and (iii) Evaluate the application of the MLR models as predictive tools to estimate the constituent EMC.

Stormwater runoff data used in Kayhanian *et al*. (2006) were obtained from 34 highway sites in California covering a wide range of annual average daily traffic levels and environmental conditions. These data were obtained, on average, up to eight storm events at each highway site during wet seasons (October to April) over a three years period (2000 to 2003). Some characteristics were recorded in each site, namely surrounding land use (obtained from United States Geological Survey maps, local zoning maps and visits to the sites), catchment area, impervious fraction, latitude and longitude and AADT.

Relationships were established by the authors between highway runoff quality for 24 constituents and the following independent variables:

(i) Total event rainfall (TER in mm) – height of rain of each precipitation event;

(ii) Antecedent dry period (ADP in days) – the number of days with no rain since the last precipitation event;

(iii) Cumulative seasonal rainfall (CSR in mm) – the total precipitation of a known season in a specific location.

(iv) Drainage area (DA in ha) – area which contributes with runoff to the discharge point during a rainfall event;

(v) Annual average daily traffic (AADT in vehicles/day) – number of vehicles that pass each day in the location under study.

The adapted version of the general equation is presented below (equation 3.4). In Table 3.7, there are the constants used in the equation.

$$\text{Ln EMC} = \beta_0 + a \times \ln(TER) + b \times \ln(ADP) + c \times \sqrt[3]{CSR} + d \times \ln(DA) + e \times (AADT \times 10^{-6}) \tag{3.4}$$

Table 3.7 – Constants Kayhanian's model (adapted from: Kayhanian *et al*., 2006)

	Constituent	**β_0**	**a**	**b**	**c**	**d**	**e**
Aggregates	TSS	4,28	- 0,124	0,102	- 0,099	—	4,934
	TDS	4,73	- 0,309	0,126	- 0,050	—	2,582
	DOC	4,11	- 0,404	0,123	- 0,129	—	—
	TOC	5,23	- 0,209	0,129	- 0,154	—	—
Metals (total)	Cu	2,9	- 0,161	0,163	- 0,079	—	6,823
	Pb	2,72	—	—	- 0,102	—	9,65
	Ni	2,51	- 0,196	0,141	- 0,075	-0,155	1,013
	Zn	4,83	- 0,227	0,143	- 0,084	—	6,747
Metals (dissolved)	Cu	2,92	- 0,290	0,185	- 0,102	—	3,679
	Pb	2,04	- 0,248	—	- 0,101	—	0,007
	Ni	2,73	- 0,270	0,068	- 0,107	-0,094	—
	Zn	4,74	- 0,343	0,164	- 0,112	—	1,676
Nutrients	NO_3-N	1,3	- 0,417	0,092	- 0,090	—	2,87
	P, total	1,2	- 0,143	0,128	- 0,051	—	0,9
	TKN	1,7	- 0,343	0,102	- 0,128	—	1,535

* The table is not complete, missing the size of the samples used, the square root of the mean error and the standard error for each constituent. These data is available in Kayhanian *et al*., 2006.

3.2.4 Stochastic Empirical Loading and Dilution Model (SELDM)

SELDM was developed by the Federal Highway Administration from the USA and uses analytical approximations to estimate the potential effects of runoff on receiving waters. SELDM aims at predicting EMC, flows and loads in stormwater from a highway site and its upstream catchment. Using input information based on site characteristics, catchment characteristics, rainfall, stormflow, water quality and the performance of mitigation measures, this tool generates statistical distribution of runoff quality in highway runoff and receiving river water (Granato, 2013a).

SELDM uses a highway runoff database which contains data from over 4000 storm events, then uses the Monte Carlo method to generate the distribution of output variables such as EMC (Gardiner *et al*., 2016).

Novotny *et al*. (1993) as quoted by Santos and Barbosa in 2004 refers that the deterministic nature of most models to represent the variability of a phenomenon has originated some failures. In this case Monte Carlo method is used due to the combination of different variables (such as precipitation, pre-storm flows, runoff coefficients and water quality concentrations).

Granato and Jones (2014) described that SELDM uses Monte Carlo methods to generate a stochastic population of the concentrations, flows and loads needed to implement a mass balance model for a receiving stream and/or lake.

SELDM is not calibrated by changing values of input variables to match a historical record of values. Instead, SELDM’s input variables are based on site characteristics and representative statistics for each hydrological variable. The benefit of this method is not to reduce uncertainty in the input statistics, but to represent the different combinations of the values of variables that determine potential risks for water quality (Granato and Jones, 2014).

To estimate the concentrations and loads of water quality constituents in receiving bodies, a mass balance is commonly applied (Granato, 2013a) as shown in Figure 3.4.

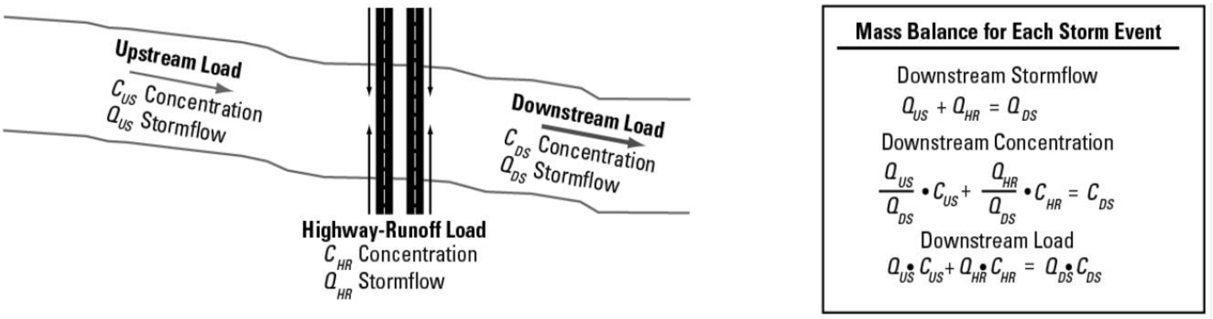


Figure 3.4 – Mass balance for each storm event (Granato, 2013a)

Storm events are commonly defined as independent statistical events characterised by a volume, intensity, duration and time between midpoints of successive storms for the purposes of planning, analysis, and sampling efforts (Driscoll, 1990 in Granato, 2013a). Statistics describing the frequency distributions of component discharges and concentrations are needed to estimate the statistics for downstream discharges, concentrations, and loads (Granato and Jones, 2014).

The fact that SELDM was designed to predict road runoff pollution in US areas represents a limitation, which is common to every national based tool. In this case, the USA model defines “Ecoregions” where the parameters are already introduced. Nevertheless, the tool can be used in every region of the world with the manually input information of weather conditions.

The input layout of SELDM is a sequence of graphical user interface (GUI). In total 13 forms need to be completed with inputs information: (1) Information about the analyst, project and analysis; (2) Highway physical characteristics; (3) Ecoregion (when the site under study is in USA); (4) Upstream basin characteristics; (5) Lake basin characteristics; (6) Precipitation statistics (when the ecoregion is settled this form is almost automatically filled, however when the site is out of USA, it is necessary to calculate these data (see Table 3.8) outside the tool); (7) Streamflow; (8) Runoff coefficient statistics; (9) Highway runoff quality statistics; (9) Upstream water quality statistics; (10) Downstream water quality definitions; (11) BMP performance statistics; (12) Set of output files and (13) Running SELDM form. As for the road runoff pollution, only two of the 13 outputs are of interest, namely: (1) Precipitation event output file and (2) Highway runoff quality output file.

SELDM offers seven options for selecting storm-event statistics on the synoptic storm-event-precipitation statistics form as supported by the appendix 4 of SELDM help guide (Granato, 2013b). The default rain zone and ecoregion are automatically selected by entering the latitude and longitude of the highway site. The user, however, can manually select an ecoregion that better represents conditions at a site of interest. The option of entering user-defined statistics can be used to enter site-specific statistics, to do a sensitivity analysis, or evaluate the potential effects of climate change on model results (Granato, 2010). In this way, it is presented in Figure 3.5 the stochastically generated event rainfall volumes and in Figure 3.6 the same values but in an ordered series.

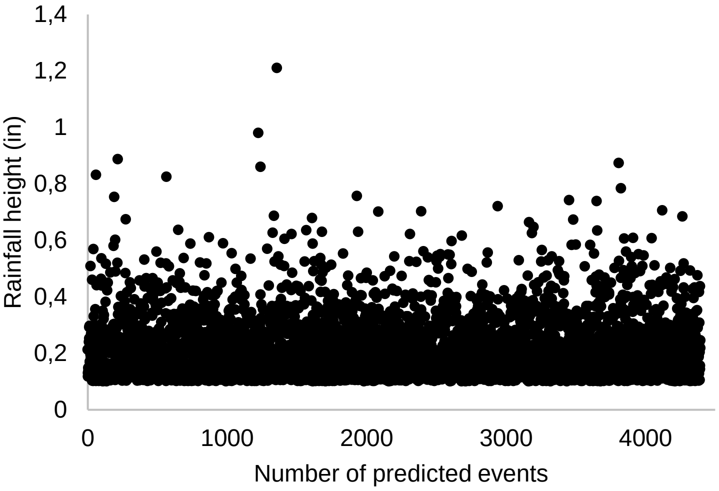


Figure 3.5 – Stochastically generated rainfall events with Portuguese data

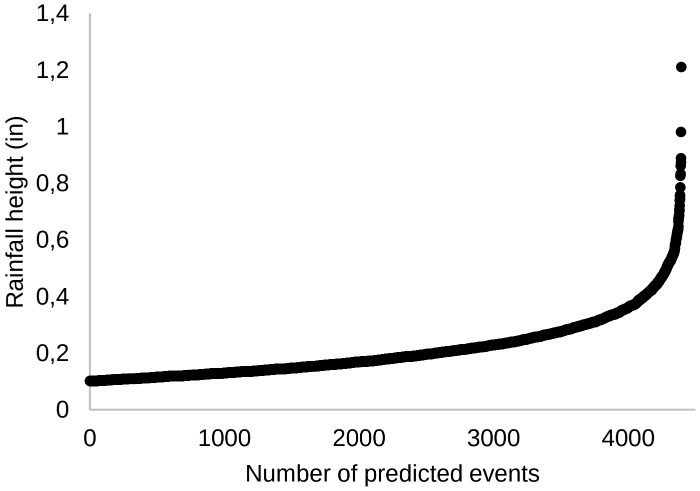


Figure 3.6 – Ordered stochastically generated rainfall event for the same site in Portugal

In order to produce highway runoff quality output file, SELDM uses regional water-quality statistics to facilitate generation of initial planning-level estimates. If necessary, initial estimates can be refined with water-quality statistics based on available data collected at hydrologically similar sites or at the site of interest. SELDM also uses the Highway Runoff Database (HRDB) as source of highway runoff statistics and data, as stated by Granato and Cazenas (2009).

The HRDB application is designed as a data warehouse to document data and information from highway-runoff monitoring studies and as a pre-processor for highway-runoff data for use in SELDM. Available highway runoff data provide the basis for defining runoff quality and quantity at monitored sites and predicting runoff quality and quantity at unmonitored sites. HRDB includes data from 2 650 storms for 39 713 EMC measurements of more than 100 water quality constituents monitored at 103 sites in USA (Granato and Cazenas, 2009).

3.2.5 Inputs and outputs summary table

In the Table 3.8 are presented the inputs which are needed to run each model.

Table 3.8 – Inputs summary table

Inputs		**Predicting tools**			
		SMC	EMC		
		PREQUALE	HAWRAT	Kayhanian's	SELDM
Site characteristics	CR		X		
	DA	X		X	X
	IF	X			X
	AADT		X	X	X
	AR	X			
	P_{annual}	X			X
	Others*	Drainage Length (m); Mean Basin Slope (%)			Location (latitude and longitude); Drainage Length (m); Mean Basin Slope; Basin Development factor
Event Characteristics	Month		X		
	TER			X	X
	MHI		X		
	ADP		X	X	X
	CSR			X	
	Others*				Average storm event durations; Minimum total storm events; Minimum interevent time; Number of storm events per year

*As indicated above, SELDM is a tool which needs more inputs than physical and characteristics ones. So, beside those here presented in Table 3.8, SELDM needs the upstream basin characteristics, basin characteristics, streamflow statistics, runoff coefficients and best management practices (BMP) used in the road.

In the Table 3.9 is presented an outputs summary table.

Table 3.9 – Outputs summary table

		Predicting tools			
		SMC	EMC		
		PREQUALE	HAWRAT	Kayhanian's	SELDM*
Aggregates	TSS	X	X	X	X**
	TDS			X	
	DOC			X	
	TOC			X	
	COD	X			
Metals (total)	Cu	X	X	X	X
	Pb			X	X
	Ni			X	
	Zn	X	X	X	X
	Cd		X		X
	Fe	X			
Metals (Dissolved)	Cu		X	X	
	Pb			X	
	Ni			X	
	Zn		X	X	
Nutrients (Total)	NO^-_3			X	X
	P			X	X
	KN			X	

* Besides these outputs, SELDM also has the following outputs: Urban TSS; Ultra Urban TSS; pH; suspended sediment concentration; Total chromium; Total Hardness

** SELDM generates as output Ultra urban TSS; Urban TSS and Non-urban TSS, in this case Non-urban TSS were used as TSS.

4 Assessment of the predicting tools

4.1 Methodology

Step 1

As presented in the previous section SELDM seems the most robust and complex model in terms of input requirements and output analysis. Since it did not result from a multi-parametric equation, a sensitivity test was carried out to verify if the methodology used in this section was adequate.

This dissertation aims to predict SMC starting only from hourly rainfall data of several meteorological stations. SELDM has its own “definition” of precipitation event fixing a minimum of 2,5 mm and an ADP of 6 hours (Granato, 2013a).

The inputs used in the sensitivity tests are presented in Table 4.1. These sensitivity tests were performed considering a reference test – Test 1, in appendix 4 of SELDM’s help guide (Granato, 2013b).

Table 4.1 – Sensitivity SELDM test inputs

SELDM Inputs			Test					
			1	2	3	4	5	6
Highway site: Identify Site Characteristics	Hydraulics	Drainage area (acres)	18,50	3,70	1,85	0,93	92,50	185,00
		Drainage length (feet)	2 000	400	200	100	10 000	20 000
		Mean Basin slope (feet per mile)	105,00	21,00	10,50	5,25	525,00	1 050,00
		Impervious fraction (0-1)	0,27	0,05	0,03	0,01	0,60	0,80
		Basin Development Factor (BDF) (0-12)	6	2	8	12	2	8
Synoptic Storm-Event precipitation Statistics	Storm-event statistics	Storm event volume (inches)	0,68	0,14	0,07	0,03	3,40	6,80
		Storm-event volume (COV)	1,06	0,21	0,11	0,05	5,30	10,60
		Storm event duration (hours)	7,72	1,54	0,77	0,39	38,60	77,20
		Storm event duration (COV)	0,90	0,18	0,09	0,05	4,50	9,00
		Time between storm events (hours)	167,00	33,40	16,70	8,35	835,00	1 670,00
		Time between storm events (COV)	1,28	0,26	0,13	0,06	6,40	12,80
		Minimum Total storm Volume (inches)	0,1	0,1	0,1	0,1	0,1	0,1
		Minimum interevent time (hours)	6	6	6	6	6	6
	Annual statistics and station count	Number of storm events per year	48,0	9,6	4,8	2,4	240,0	480,0
		Number of storm events per year (COV)	0,27	0,05	0,03	0,01	1,35	2,70

After running the tests, it was possible to determine the SMC for each test. The highway quality runoff output returns a series of storm events as explained in the section 3.2.4, and the pollutant EMC for each storm event. In Figure 4.1 is presented the results from the sensitivity tests.

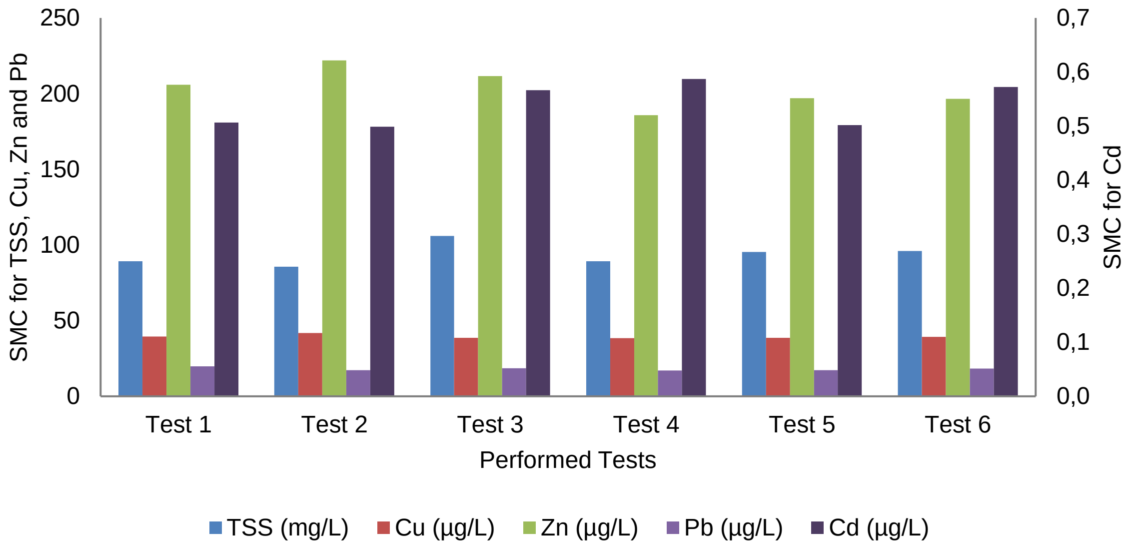


Figure 4.1 – SMC of each test performed in the sensitivity test

Besides great variations in the input values for tests one to six, SELDM results of road runoff pollutant concentrations do not show great changes. This was an aid to the development of modeling with SELDM. Due to the high number of inputs required to run the program, and due to some difficulty in sometimes obtaining all these inputs from all project partners, it was possible to model some highways which were missing one or two input values, by using values that were consistent with the characteristics of the studied site.

Step 2

Since the average of the EMC of each event resulting from the output does not show great changes, a second approach to the same model was attempted. The case study of a Portuguese highway - A25 at Gafanha da Nazaré - which was previously monitored by Antunes (2014), was implemented in SELDM in order to compare monitored and predicted events. The model predicted 1346 events along with the precipitation characteristics of each event. The characteristics considered for the initial comparison between predicted (1346) and monitored (30) events were the rainfall volume, ADP and event-duration. From the 30 monitored events, 23 had at least one predicted event match, i.e. the values of the characteristics referred above were similar. On the other hand, there was no predicted event which matched the remaining seven monitored events. The second comparison was regarding the SMC. Like so, the 23 monitored events were compared with each matched predicted event and the results are present in Figure 4.2. Besides the fact that the deviation between monitored and predicted SMC values was not very large, it was noticed that the EMC values that were used to calculate the SMC, do not appear to have great similarity.

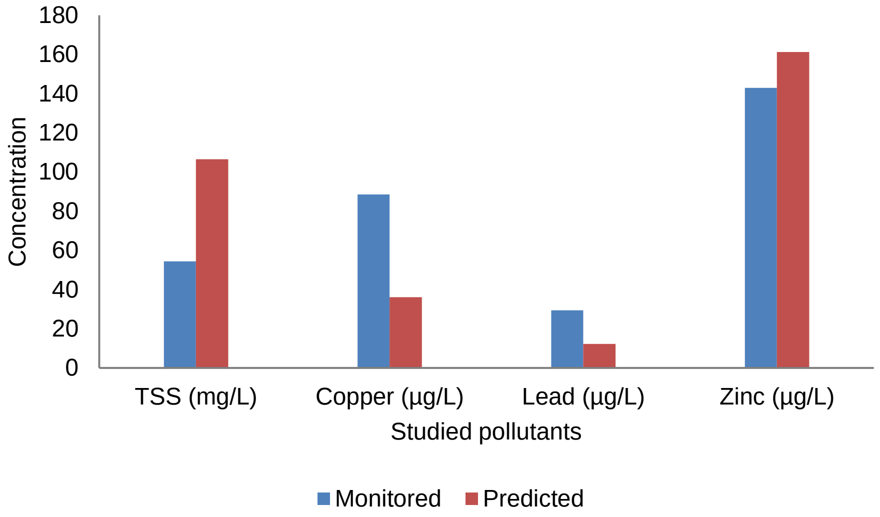


Figure 4.2 – Comparison of A25 results for monitored and predicted concentration through similar events

After these two analyses, it was decided that the analysis of the results would be made considering all the outputs of the tool to each pollutant and then the average of all the EMC. After that, the following steps were followed:

Step 3

Before the prediction with the models, the monitored SMC were calculated for each pollutant of each road. The method used was independent from the number of monitored samples. The monitored EMC were averaged as shown in equation 2.2 and is presented in Table 3.2.

Step 4

An Excel spreadsheet was developed in order to calculate input data of HAWRAT, Kayhanian's model and PREQUALE. Following the recommendations of HAWRAT's help guide: in this spreadsheet it was assumed that a precipitation event is every event above 0,1 mm. The procedure for the development of this spreadsheet was:

(i) Collect the hourly precipitation time series from the closest meteorological stations of each site[3]; Identification of all precipitation events. A precipitation event was considered as every precipitation associated to an hour or several hours with at least 0,1 mm as indicated by HAWRAT's help guide. According to the example in Figure 4.3, this definition lead to the identification of four "precipitation events" in that interval, two of which were only one hour and the other two were two and three hours.

---

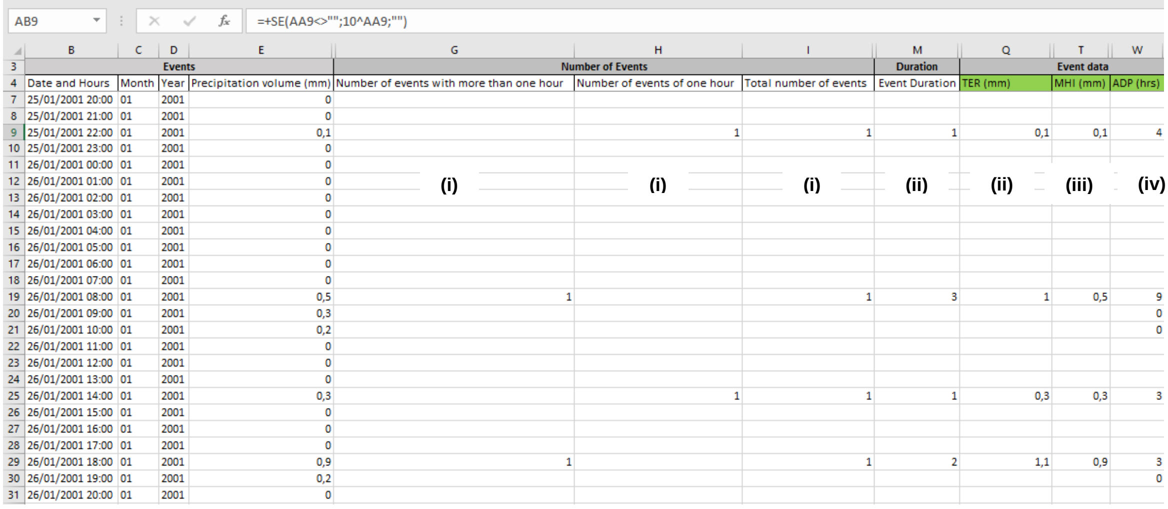
[3] Portugal - https://snirh.apambiente.pt
Netherlands - https://www.knmi.nl/home
Norway – http://eklima.met.no
France – http://www.meteofrance.com/accueil
Ireland – https://www.met.ie/
United Kingdom - Moy and Crabtree, 2002a; Moy and Crabtree, 2002b; Moy and Crabtree, 2002c; Moy and Crabtree, 2002d; Moy and Crabtree, 2002e; Moy and Crabtree, 2002f

(ii) The calculation of each precipitation event duration was essential for the total event rainfall (TER) calculation, because the calculation of this input requires the number of hours that are needed to be summed.

(iii) Obtain the maximum hourly precipitation (MHI) value from each event. This value was calculated by finding the maximum value of each event in the hourly precipitation series, using as auxiliary calculation the column that identifies an event and the duration of each event.

(iv) Calculation of the antecedent dry period (ADP) of each event by calculating the number of empty cells until the last event.

All the procedure above mentioned is available in Figure 4.3.



AB9

=+SE(AA9<>"";10^AA9;"")

	B	C	D	E	G	H	I	M	Q	T	W
3	Events				Number of Events			Duration	Event data		
4	Date and Hours	Month	Year	Precipitation volume (mm)	Number of events with more than one hour	Number of events of one hour	Total number of events	Event Duration	TER (mm)	MHI (mm)	ADP (hrs)
7	25/01/2001 20:00	01	2001	0							
8	25/01/2001 21:00	01	2001	0							
9	25/01/2001 22:00	01	2001	0,1		1	1	1	0,1	0,1	4
10	25/01/2001 23:00	01	2001	0							
11	26/01/2001 00:00	01	2001	0							
12	26/01/2001 01:00	01	2001	0							
13	26/01/2001 02:00	01	2001	0							
14	26/01/2001 03:00	01	2001	0							
15	26/01/2001 04:00	01	2001	0							
16	26/01/2001 05:00	01	2001	0							
17	26/01/2001 06:00	01	2001	0							
18	26/01/2001 07:00	01	2001	0							
19	26/01/2001 08:00	01	2001	0,5	1		1	3	1	0,5	9
20	26/01/2001 09:00	01	2001	0,3							0
21	26/01/2001 10:00	01	2001	0,2							0
22	26/01/2001 11:00	01	2001	0							
23	26/01/2001 12:00	01	2001	0							
24	26/01/2001 13:00	01	2001	0							
25	26/01/2001 14:00	01	2001	0,3		1	1	1	0,3	0,3	3
26	26/01/2001 15:00	01	2001	0							
27	26/01/2001 16:00	01	2001	0							
28	26/01/2001 17:00	01	2001	0							
29	26/01/2001 18:00	01	2001	0,9	1		1	2	1,1	0,9	3
30	26/01/2001 19:00	01	2001	0,2							0
31	26/01/2001 20:00	01	2001	0							

Figure 4.3 – Spreadsheet model to calculate model’s inputs. The boxes with numbers refers to the bullets in the steps (i) to (iv) above

(v) After all the event variables were calculated, EMC were calculated for each one precipitation event.

(vi) Calculation of the annual precipitation height. This value was calculated averaging the annual precipitation time series. Due to the lack of data, for Norway the annual precipitation was the average precipitation per year from the hourly precipitation series.

(vii) Calculation of the cumulative seasonal rainfall (CSR). For the calculation of this variable, the year was divided into four seasons: (i) December, January and February; (ii) March, April and May; (iii) June, July and August and (iv) September, October and November. For each season, it was assigned a characteristic value. This value was obtained by the sum of all the precipitation that had occurred in one of the three months of each season.

(viii) The last variable calculated in the Excel spreadsheet was the AR. This variable is very important as it has great influence in the prediction of PREQUALE.

The explanation of how to calculate the AR was already in the description of PREQUALE (see section 3.1.2). In order to obtain the variable, and after having the IDF curve with two years of return period, it is only necessary to multiply the value of t_c, calculated through equation 3.2 to the value in minutes of the IDF curve.

(ix) In order to calculate EMC for each event in the Excel spreadsheet, some physical characteristics of each site were still necessary, such as: DA, AADT, IF, DL, S and CRC.

Step 5

Calculation of the predicted SMC. Equation 2.2 was applied for the predicted EMC for each pollutant in the spreadsheet (for HAWRAT and Kayhanian's model) and in the SELDM outputs.

Step 6

Comparison of SMC for each highway and pollutant. This comparison was performed considering the four studied tools and the monitored data in each highway. Thus, it was possible to check which tool best predicts SMC at each highway. These results are presented in section 4.4.

Step 7

The accuracy of each model was evaluated considering the following indices (Trenouth and Gharabaghi, 2016):

The coefficient of determination (R^2) is defined as the squared value of the coefficient of correlation according to Bravais-Pearson. This coefficient estimates the combined dispersion against the single dispersion of the observed and predicted series. The range of this coefficient lies between 0 and 1 which describes how much of the observed dispersion is explained by the prediction. A value of zero means no correlation whereas a value of one means that the dispersion of the prediction is equal to the observation (Krause *et al*., 2005).

The fact that the coefficient only calculates the dispersion of the forecast, is the main reason why this coefficient could not be studied as the only error indices of a model. If R^2 was in any case the only error to validate a model it is necessary to consider the gradient and the intercept of the regression (Krause *et al*., 2005).

$$R^2 = \left[\frac{\sum_{i=1}^{n}(O_i - \bar{O})(P_i - \bar{P})}{\sqrt{\sum_{i=1}^{n}(O_i - \bar{O})^2} \times \sqrt{\sum_{i=1}^{n}(P_i - \bar{P})^2}}\right]^2 \tag{4.1}$$

R^2 – Coefficient of determination;

n – number of SMC under evaluation;

O_i – Observed value;

$\bar{O}$ - Average of the observed values;

P_i – Predicted value;

$\bar{P}$ - Average of the predicted values;

The E_{NS} coefficient which was proposed by Nash and Sutcliffe in 1970 (Krause *et al.,* 2005) and assesses the predictive power of the model. Typically, a value of E_{NS} of 0,75 or greater is understood as a result of a good model to predict road runoff. If the value is equal to 1, it is seen as a perfect prediction model (Trenouth and Gharabaghi, 2016). For the case of regression procedures this coefficient is equivalent to R^2.

$$E_{NS} = 1 - \frac{\sum_{i=1}^{n}(O_i - P_i)^2}{\sum_{i=1}^{n}(O_i - \bar{O})^2} \tag{4.2}$$

The coefficient of residual mass (CRM) which assess prevalent over-estimation or under-estimation of the observed values, and for a well-performing model should approach a value zero (Trenouth, 2017).

$$CRM = \frac{\sum_{i=1}^{n} O_i - \sum_{i=1}^{n} P_i}{\sum_{i=1}^{n} O_i} \tag{4.3}$$

The RMSE describes the differences between the observed and predicted values in the units of the variable of study, and is an additional term used to characterise a model performance. This error is always non-negative and the zero value would mean a perfect fit data (Trenouth, 2017).

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n}(P_i - O_i)^2}{n}} \tag{4.4}$$

4.2 Input Data

In Table 4.2, the physical characteristics that serve as input of the studied models are presented. In this table, the reference to each one of the highways was made through a code that was firstly presented in Table 3.1.

Table 4.2 – Physical characteristics of road used as inputs in the tools

Highways	**CR**	**DA** (m^2)	**DL** (m)	**S** (%)	**IF** (0-1)	**BDF** (0-12)	**P_{annual}** (mm)	**AR** (mm)	**AADT** (no. vehicles)
P1	Warm/Wet	22 800	814	2,95	0,412	6	645,95	7,80	27 746
P2	Warm/Wet	1 287	117	7,70(c)	1,000	6	527,98	6,00	16 344
P3	Warm/Wet	5 580	465	3,00(c)	1,000	6	744,43	5,50	2 918
P4	Warm/Wet	15 422	612	3,40(c)	0,850	6	518,33	7,00	24 000
P5	Warm/Wet	287	25	2,50	1,000	6	1 013,76	6,00	15 673
P6	Warm/Wet	7 280	520	3,30(c)	1,000	6	708,61	6,00	6 539
N1	Warm/Dry	48 590	1 600	0,20(c)	0,500(d)	6	776,00	3,67	63 000
N2	Warm/Dry	30 510	2 700	0,20(c)	1,000	6	776,00	6,00	63 000
N3	Cold/Dry	22 000	1 630(b)	3,40(c)	1,000	6	834,42(e)	2,50	42 000
F1	Warm/Wet	3 200	275	2,50	1,000	6	786,00	9,00	24 103
F2	Warm/Wet	3 200	275	2,50	0,500(d)	6	786,00	9,00	24 103
I1	Cold/Wet	14 184	1 200	0,94	1,000	6	731,00	3,80	27 500
I2	Cold/Wet	11 368	480	0,50	1.000	6	731,00	3,80	27 500
I3	Cold/Wet	9 600	800	0,50	1,000	6	731,00	3,80	27 500
E1	Warm/Wet	8 755	724	1,10(c)	1,000	6	745,20	2,08	70 000
E2	Warm/Wet	4 348(a)	303	0,66(c)	1,000	6	745,20	1,48	35 000
E3	Warm/Dry	58 680	1 800	2,40(c)	1,000	6	614,80	3,27	78 000
E4	Warm/Wet	20 232	735	3,10(c)	1,000	6	843,40	1,55	24 000
E5	Warm/Wet	2 760	250	0,80(c)	1,000	6	659,70	1,19	64 000

Highways	CR	DA (m^2)	DL (m)	S (%)	IF (0-1)	BDF (0-12)	P_{annual} (mm)	AR (mm)	AADT (no. vehicles)
E6	Warm/Wet	19 425	1 050	0,19(c)	0,500(d)	6	635,40	5,90	36 000
Range	**Minimum**	287	25	0,19	0,412	6	527,98	1,19	2 918
	Maximum	58 680	2 700	7,70	1,000	6	1 013,76	9,00	78 000

The monitored data is available in: Barbosa and Fernandes, 2012; Leitão *et al.,* 2005; Antunes, 2014; Barbosa, 2007; Brongers, 2011a; Brongers, 2011b; Vollertsen *et al.,* 2007; Mufleh et al., 2010; Higgins, 2006; Moy and Crabtree, 2002a; Moy and Crabtree, 2002b; Moy and Crabtree, 2002c; Moy and Crabtree, 2002d; Moy and Crabtree, 2002e; Moy and Crabtree, 2002f.

The IDF curves used as AR auxiliary calculations are available at: Brandão *et al.,* 2001; Korving *et al*., 2009; http://eklima.met.no; EDF-DTG and Cemagref, 1993 and https://www.met.ie.

(a) Estimated drainage area by multiplying the length by the section width

(b) Estimated drainage length by dividing the available area by the width consulted in Google Earth Pro

(c) Estimated slopes through the Google Earth Pro function, elevation profile

(d) Assumed impervious fraction

(e) Assumed P_{annual}

It should be noted that there were some difficulties gathering all the input data. It was necessary to estimate some of the inputs as explained in Table 4.2.

Starting in the first column, it can be verified that a climate region was assigned to each highway studied. This is due to the fact that in this work it was considered that the red lines that limit each climatic region in HAWRAT (only for United Kingdom), were extended in the direction they end to the model (Figure 3.3).

Regarding the drainage area there were not many problems, since the documents referring to each highway, described this characteristic except on the E2, where the determination of the area had to be made by multiplying the length of the section by the width.

In the drainage length column, only N3 did not have the value available to the development of the work. In this case, it was possible to estimate this value, since the area is available as the width was consulted in Google Earth. The same software was used to estimate the missing slopes through the elevation profile function. The estimated slopes are marked in the table with an asterisk.

Regarding the values of impermeable fraction, N1, F2 and I6 have the values of 0,5. This is due to the fact that in the reports in which the study was based, it is only referred that the highways have permeable asphalt. So, the impermeable fraction was considered as 0,5.

In order to have one input that was only needed to run SELDM, it was necessary to estimate a value for BDF. It was decided to consider a value of six for all the highways for two reasons: (i) documents related to the highways characteristics did not have much information in relation to the surrounding lands (forest, bushes, intensive farming, among others) and (ii) in SELDM sensitivity test, several BDF values have been tested, and no great variation was verified.

The annual precipitation was already calculated through the average of annual precipitation data to each site. The only highway which annual precipitation was calculated through the hourly precipitation data was N3 due to the lack of data.

To calculate AR (for PREQUALE), IDF curves were needed. These curves were available for road located in Portugal, Norway, Ireland and Netherlands. For England, it was used an IDF curve which belongs to the Bristol city and for France only one IDF curve for the province of Alps was available.

4.3 Comparison of the predictions

In the first part of this section the comparison between predictions and monitored values are presented in the Figure 4.4.

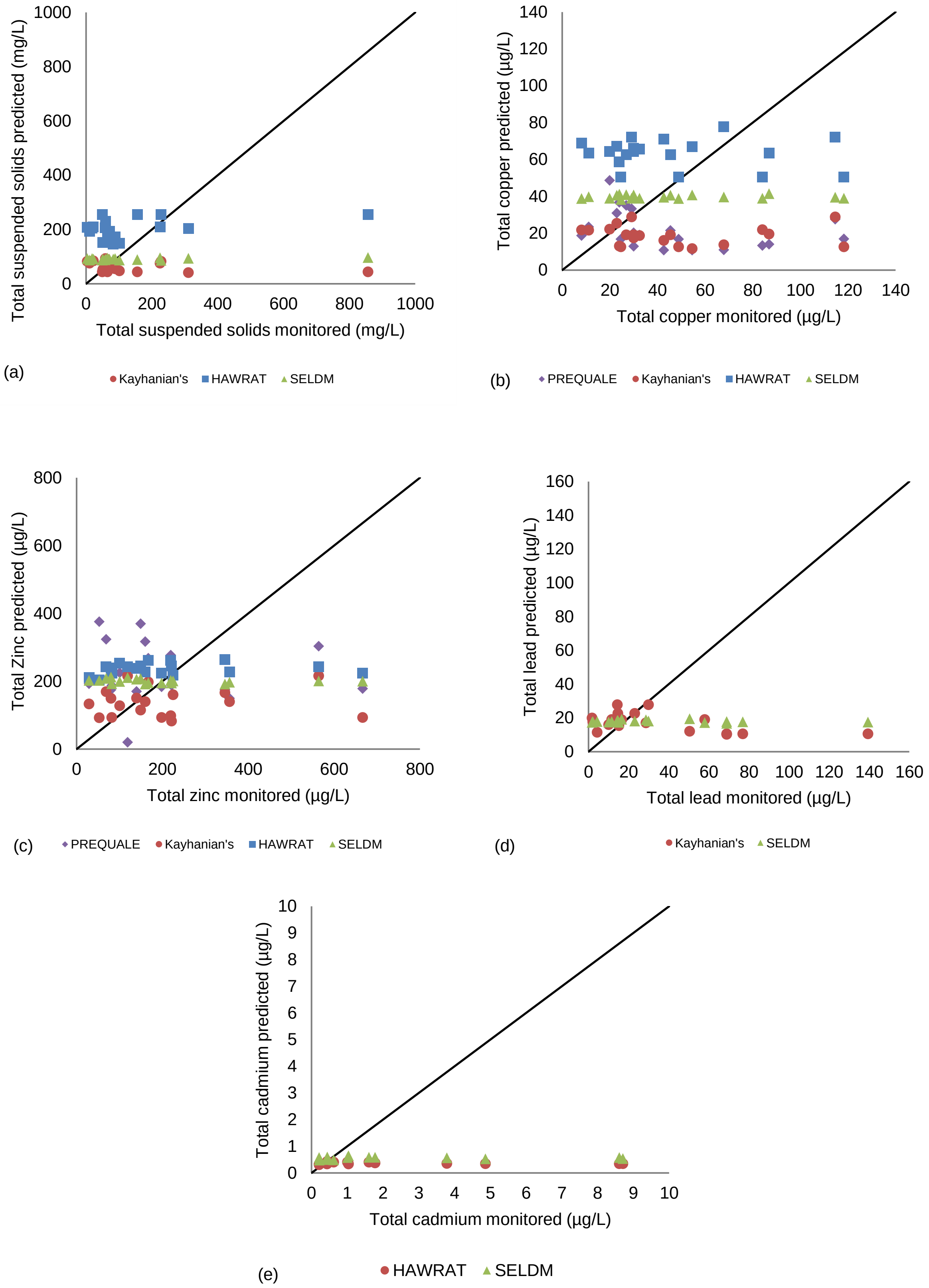


Figure 4.4 – Comparison SMC monitored and predicted (a) TSS; (b) copper; (c) zinc; (d) lead and (e) cadmium

At first glance, it is easily observed that any of the models is robust enough to predict road runoff pollution, to the European roads. None of the models predicts the variation of the monitored values. Moreover, none of the models results vary much with great variations of monitored data, which indicates that the models do not possess great sensitivity to the input variations. To corroborate this visual analysis, the error indices were calculated (Table 4.3) and analysed. It is important to notice that although PREQUALE is able to predict TSS, the results of this prediction are not available in the Figure 4.4, because the results are very disperse and very high, thus the graphical representation of these would not allow the visualization of the remaining results.

Table 4.3 – Error indices table

		Error Indices			
		R^2	**E_{NS}**	**CRM**	**RMSE**
TSS	HAWRAT	$1,682\times10^{-1}$	-0,008	-0,500	193,517
	Kayhanian	$1,468\times10^{-1}$	-0,216	0,524	212,501
	SELDM	$1,803\times10^{-1}$	-0,041	0,329	196,671
Copper	PREQUALE	$1,219\times10^{-1}$	-0,916	0,523	43,549
	HAWRAT	$2,090\times10^{-2}$	-0,435	-0,377	37,692
	Kayhanian	$1,900\times10^{-3}$	-0,792	0,591	42,112
	SELDM	$4,000\times10^{-4}$	-0,042	0,137	32,123
Zinc	PREQUALE	$8,700\times10^{-3}$	-0,377	-0,077	193,738
	HAWRAT	$1,110\times10^{-2}$	-0,021	-0,142	166,839
	Kayhanian	$7,200\times10^{-3}$	-0,192	0,330	180,262
	SELDM	$6,850\times10^{-2}$	-0,023	0,032	166,973
Lead	Kayhanian	$2,890\times10^{-1}$	-0,461	0,509	42,047
	SELDM	$5,750\times10^{-2}$	-0,254	0,488	38,961
Cadmium	HAWRAT	$1,270\times10^{-2}$	-0,658	0,866	3,778
	SELDM	$3,900\times10^{-3}$	-0,5510	0,7957	3,6541

Four error indices were used in order to evaluate the performance of the models. The analysis of the Table 4.3 was made by error index:

(i) The highest R^2 was of 0,28 which is a very low value to guarantee a robust model. However, this information is not enough since it only allows to conclude about a tendency between monitored and predicted data. This means that a high R^2 could be obtained even if the predicted data was very different from the monitored data, as long as there was a linear tendency.

(ii) Although both visual and coefficient of determination analysis show the models were not robust enough, the efficiency coefficient (E_{NS}) was still analysed to assess overall model efficiency and the previous analysis. Since all values were below 0,5, it can be concluded that the model is not robust, as previously suggested by the coefficient of determination analysis.

(iii) Regarding the CRM, most values were not close to zero. This may suggest an under prediction, in the case of positive values, or an over prediction in the case of the negative values. There was one exception: zinc concentration prediction through SELDM which presents and CRM of 0,0321. Still, looking at the graphical representation (Figure 4.4) it is observable that the relation between predicted and monitored data is not satisfactory. Hence, CRM is not enough to determine if a model is well adjusted to the data.

(iv) Regarding RMSE, all of indices calculated are much larger than zero (>32 µg/L or >193 mg/L in the case of TSS), except for cadmium (<4 µg/L). Still, in this case, the error is considered big since the average of the observed data (2,74 µg/L) is lower than the error index, which indicates that the error is significant.

4.4 Critical review of the models

PREQUALE is a very simple tool of direct application and does not present great problems. In order to obtain the necessary data to run the model, almost all the data are also easily obtainable, except one input, the AR. This input requires some data to be obtained for intermediate calculations that are not always available in previously monitored locations such as the length of the drainage section and the variation in height. In addition to these two inputs, the final stage of this input calculation involves the use of an IDF curve of the site, which has become quite complicated to obtain. Indeed, the results may be biased since it was not possible to use the correct IDF curve for UK and France.

HAWRAT is easy to apply having only one input that makes it difficult to apply at European level. For the application of this model it is necessary to indicate the climatic area for each road. However, it only sets out the zones for the United Kingdom, being necessary an adaptation if it is intended to simulate outside UK.

As PREQUALE and HAWRAT, Kayhanian’s model only had one input that made it difficult to use. This model uses as input the CSR, which is a variable that is not widely used in Europe, and it was difficult to decide how it should be analysed. It was decided that only four seasons of the year would be considered.

SELDM was the hardest model to work. This model was the only one which used a complex graphical interface. SELDM has several forms to fill with a lot of mandatory inputs and part of them is difficult to obtain, like BDF.

Another feature that makes SELDM more difficult to apply than the other models is its increasing difficulty of use when the model is being applied outside the USA. For the USA, the precipitation data is not needed as input, because by setting the highway location, SELDM automatically fills these data. If the case study is outside of the USA, which is the case, it is needed to complete several precipitation statistics as indicated in the second chapter of the annexes.

Although these models had shown great robustness in previous studies (*e.g*. Barbosa, 2007; Barbosa *et al*. 2011; Dempsey and Song, 2008; Kayhanian *et al*., 2006 and Granato and Jones, 2015), this was not observed in the present work. The greater robustness in those studies could be possibly explained by the fact that each model was tested in sites that are geographically similar to the ones that were used to calibrate them.

The Table 4.4 is presented below in order to show the pros and cons of each model.

Table 4.4 – Table regarding the pros and cons of each model

Models	Pros	Cons
PREQUALE	Easy to calculate; ADP is not used in PREQUALE. It seems to be an advantage since no correlation between road runoff concentration and ADP was noticed by Leitão *et al*. (2005), in portuguese and international studies. Predict SMC instead of EMC, which is assumed as a benefit in Leitão *et al.* (2005).	The number of monitored roads used to construct the model (six), does not represent a robust quantity and diversity of road characteristics that may be characteristic from all Europe; The model was created from a regression analysis that is only based on four variables. Average annual rainfall volume with the same duration as the basin time of concentration (AR), was very hard to find in the monitored data from Europe.
HAWRAT	Easy to calculate; Input data easily available for users; Calibrated with a robust number of monitored roads for UK, which results in good predicting results (Dempsey and Song, 2008).	Besides the fact that this model was based in more monitored sites than PREQUALE, the characteristics variability in order to apply to all Europe is very low; HAWRAT does not appear to have sensitivity to great variations of SMC, being very constant from site to site.
Kayhanian	Easy to calculate; Input data easily available for users.	The model was built based entirely on roads from a specific site from the USA and besides the great number of roads studied, the roads studied do not have the variability that is needed to study SMC in an European level; Based in the visual analysis, this method does not appear to have a direct relation between monitored data and predicted data for the highest values of the monitored data.
SELDM	The model defines a range of values where the output should be; The capability to insert precipitation data manually, allows the user to predict road runoff in a climate change scenario.	In order to evaluate SMC individually, this model is not efficient based on the data observed in this work. However, this model works in a way that is different from the others which may be the best way to define highway pollution. This model assumes a range where the pollutant concentration is in most of the times, and define that value as the average of the output.

After the analysis of the results of these four models, it was possible to conclude that none of the models was robust enough to be applied to European roads.

5 Proposed model

5.1 Development of a new model

Considering the gathered monitored data and the poor performance of the predicting models, the development of a new model is proposed.

The proposed model uses a multiparametric equation that allows the user to predict SMC for TSS (mg/L), copper (µg/L), zinc (µg/L), lead (µg/L) and cadmium (µg/L). This model is based on the following principles: (i) input data easily available for the user; (ii) easiness of calculation and (iii) more robust results for Europe as a whole than the previously studied tools.

In order to accommodate the several factors that may influence the pollutant concentrations, the following variables were considered to the model:

(i) Drainage area (DA in m^2) – Area that contributes to the runoff;
(ii) Drainage length (DL in m) – Length of the road;
(iii) Impervious fraction (IF in 0-1) – The fraction of the DA that is impervious;
(iv) Annual precipitation (P_{annual} in mm) – The average of annual precipitations of each site;
(v) Annual average daily traffic (AADT in nº of vehicles) – The number of vehicles that pass daily in the site.

The multiparametric equation takes the following form:

$$LN\ (SMC) = \delta_1 + \delta_2 \times DA + \delta_3 \times DL + \delta_4 \times IF + \delta_5 \times P_{annual} + \delta_6 \times AADT \quad (5.1)$$

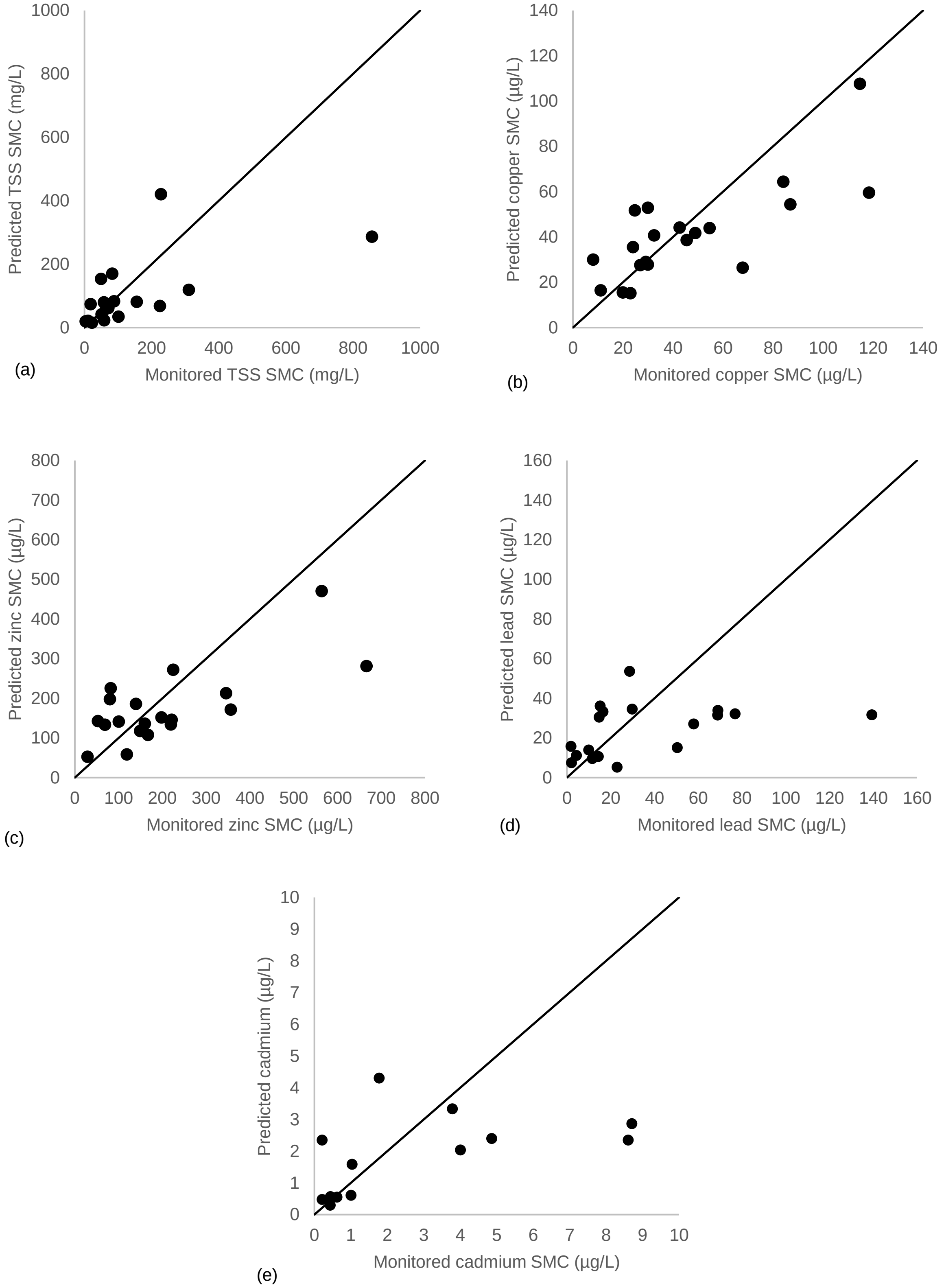
Where the SMC is given through the form of a natural logarithm. This model was calibrated with the characteristics of the roads that were presented in Table 4.2 and the regression and correlation coefficients that resulted from the adjusted multiparametric equation of the roads SMC are presented in Table 5.1. It is important to emphasize that for the development of this equation it was not took into account which are the variables with more weight, because the main objective was to have an equation with the most easily obtainable parameters.

Table 5.1 – Correlation coefficients

	δ_1	δ_2 **(DA)**	δ_3 **(DL)**	δ_4 **(IF)**	δ_5 **(P_{annual})**	δ_6 **(AADT)**
TSS (mg/L)	-0,803916	-0,000026	0,001846	2,089499	0,003128	-0,000007
Copper (µg/L)	0,677390	-0,000019	0,000570	0,672196	0,002530	0,000005
Zinc (µg/L)	4,101014	-0,000041	0,001018	0,455414	0,000785	-0,000009
Lead (µg/L)	-2,333752	-0,000006	0,000032	2,070897	0,004048	0,000009
Cadmium (µg/L)	-6,595958	0,000033	0,000118	3,342029	0,004994	-0,000023

5.2 Results and performance evaluation

In the first part of this section are presented the predictions in Figure 5.1.



(a) (b) (c) (d) (e)

Figure 5.1 – Comparison of the predicted and monitored data of (a) TSS; (b) Copper; (c) Zinc; (d) Lead and (e) Cadmium

By the visual analysis of Figure 5.1, it can be observed that the predicted values follow the tendency of the monitored values. The correlation between predicted and monitored seems stronger than the ones obtained for the four models studied previously. Still, there are some differences between pollutants. This correlation seems to be stronger for copper and zinc than for the remaining pollutants.

After the development of the new model it was necessary to check its validity through the calculation of the errors that were used to evaluate the performance of the four tools studied (Table 5.2):

Table 5.2 – New model error indices

		Error Indices			
		R^2	E_{NS}	CRM	RMSE
New model	TSS	0,355	0,317	0,258	159,298
	Copper	0,584	0,548	0,107	21,142
	Zinc	0,511	0,447	0,154	122,772
	Lead	0,156	0,053	0,317	33,865
	Cadmium	0,260	0,154	0,333	2,698

(i) Regarding the R^2 it was noticed that none of the values were close to 1. However, in comparison to the models studied previously, this model presents much higher R^2, except for lead.

(ii) None of the parameters achieved the perfect value of E_{NS} (E_{NS}=1), however two of the indices indicate a reasonably good performance (copper and zinc).

(iii) For a perfect performance of the model, the CRM must be zero which is not the case. The positive values show that the model under-estimates the SMC.

(iv) Concerning RMSE, all indices calculated are much larger than zero except for cadmium (2,70 µg/L). Still, in this case, the error is considered big since the average of the observed data (2,74 µg/L) is very close to the error index, which indicates that the error is very large.

5.3 Critical review of the model

The developed model has some characteristics which are critically reviewed in this section:

(i) This new model is a multiple linear regression equation and is based on five variables (DA, DL, IF, P_{annual} and AADT) that were chosen only based on availability of the variables for each road;

(ii) AADT is one of the input variables. No clear correlation was found by the FHWA (1996) (in Leitão *et al*. 2005) between this variable and the quality of road runoff. In this way, it was concluded by Leitão *et al*. (2005), that every model that is based only in this variable should be carefully evaluated. However, it was already shown during this work that the parameters used to calculate road runoff pollution are still not widely established, as referred in the section 2.1.1, where it is said that Irish *et al*. (1995) consider the AADT as one of the three parameters regarding the volume of traffic;

(iii) This tool presents limitations based on the few data that support the construction of the regression equation. This equation was only based on the data studied in the present dissertation.

(iv) The data for which the model was tested were the same as those used for the calibration.

6 Conclusions and further work

The evaluation of the road runoff predicting tools is very important to understand the environmental impact caused by road runoff (diffuse pollution). In a broader view, the control of road runoff pollution may also help the conservation of the receiving water bodies (*e.g.* reduction of runoff pollutant concentration entering to a reservoir, which may lead to an decrease of the cost in the operation of drinking water treatment).

In this work, it was possible to obtain a better understanding of the pollutant characteristics of some European roads through the collection and analysis of several monitored events. With this, it was possible to conclude that the SMC of most pollutants in all roads were below the emission limit defined by the Portuguese Decree-Law n.º 236/98, from 01 August, except for TSS. This pollutant showed to be above this limit several times, which should be considered in the management of and possible treatment of this pollutant.

Regarding the study of the predicting tools, it was possible to conclude that none of the models was robust enough to be applied to European roads as a whole. This could be explained by the monitored data used to calibrate each model. Apart from SELDM each model is focused in limited geographical boundaries. Summing up, the following conclusions can be drawn for each model:

(i) PREQUALE is a very interesting model. It is simple to use; all the input data is reasonably easy to get and apply and the regression parameters used were chosen through a principal component analysis. However, this tool was only calibrated for Portugal and even for this country, this model is not complete, as it was assumed by the authors which indicate that it needs to be continuously updated.

(ii) HAWRAT is also a rather user-friendly model with easy application, however this model aims at predicting EMC. The probable reason for this model to not produce robust values in Europe is the same as PREQUALE. This model was only based on monitored roads from UK which may have specific characteristics.

(iii) Kayhanian’s model presents the same characteristics of PREQUALE and HAWRAT, mainly since all three models are based in one equation (per pollutant). Kayhanian’s model was calibrated with monitored data from California, which could be similar to Portugal in climate conditions but is not similar to the rest of the countries studied.

(iv) SELDM is a quite different model. This model presents a much more complex GUI than HAWRAT. This model is based on a data set of precipitations and previous monitored data. After the selection of one area (the model divides the USA in several *Ecoregions*), it stochastically predicts precipitation event series. Then, each event has several quality and precipitation parameters (*e.g.* concentrations and rain height) associated. The output series for each pollutant is very similar even with very different roads, which may explain that the model tries to define an approximated SMC. However, the defined value by the model is very different than the averages presented by the monitored data studied throughout this work.

It could be said that the main reason that affects the imprecisions of road runoff prediction in Europe is the fact that the models were calibrated to a defined country or region.

Moreover, it should be recognized that the two more complex models, HAWRAT and SELDM have a broader application than just predict pollutant concentrations. As explained in section 3.2, these two models have different steps and their ultimate objective is the evaluation of the impact of the road runoff in the receiving water bodies and the need for treatment systems. Therefore, the road runoff prediction is a small part of these models.

Since the results were not satisfactory, a new regression model was developed. This model was developed with a regression of several variables, which serve as input of the model. The choice of the variables was made considering essentially their availability to the users. The roads used to construct the regression and to test the model were the same. This model will gain some robustness if more monitored data could be used to calibrate it. In this way, the best way to predict road runoff concentrations could be to take advantage from the knowledge already existent in Europe (in this case from Portugal and UK) to use and construct models for each country instead of trying to creating a general model for all Europe.

Regarding the data of the predicting models, the conclusion is that in the highways runoff the climatic characteristics and land use have as much or more impact than some of the variables usually studied in the models.

If the perspective is to build a model that serves all Europe, some considerations should be taken in the future: (i) Build a SMC regression model for each Köppen-Geiger area or (ii) continue the PREQUALE process, for Portugal and Europe. PREQUALE was developed based on a principle components analysis, and predicts SMC as it is advised by some specialists. Some authors defend that the road runoff concentration out of the urban areas does not vary much with the ADP. In this way, PREQUALE with more monitored data could achieve a determination coefficient for each pollutant, much better than the one presented in this work. After the improvement of these tools or after obtaining the largest number of monitored data possible, it would be possible to define which is the best model to be applied in Europe and start to develop some complementary studies that may allow the European environmental and traffic agencies perform robust environmental evaluation.

7 References

Abdel-Shafy, H.I., Mansour, M.S.M. (2015). A review on polycyclic aromatic hydrocarbons: Source, environmental impact, effect on human health and remediation. Egyptian Journal of Petroleum. 25(1), 107-123. https://doi.org/10.1016/j.ejpe.2015.03.011

Antunes, P.A.S.B.M. (2014). O efeito da deposição salina nas características das escorrências rodoviárias em zonas costeiras. PhD Dissertation, University of Minho. Retrieved from: http://repositorium.sdum.uminho.pt/handle/1822/40554

Barbosa, A.E. (2007). Establishing a procedure to predict highway runoff quality in Portugal. G.M. Morrison and S. Rauch (eds.), Highway and Urban Environment: Proceedings of the 8th Highway and Urban Environment Symposium, 371–383. https://doi.org/10.1007/978-1-4020-6010-6_33

Barbosa, A.E., Fernandes, J.N. (2012). Comparison of the pollutant potential of two Portuguese highways located in different climatic regions. Rauch S., Morrison G. (eds). Science and Technology: Tools for Sustainable Development, Vol. 19. https://doi.org/10.1007/978-94-007-2540-9_24

Barbosa, A.E., Telhado, A., Caliço, J., Fernandes, J., Vieira, J., Almeida, L. V., Whitehead, M., … Baguinho, R. (2011). Directrizes para a Gestão Integrada das Escorrências de Estradas em Portugal. National Laboratory for Civil Engineering. Lisbon. Portugal: Europress, Lda.

Brandão, C., Rodrigues, R., & Costa, J. P., (2001). Análise de Fenómenos Extremos Precipitações Intensas em Portugal Continental. Water Resources Services Board, Lisbon.

Brongers, I. (2011a). Jaarverslag 2010 monitoring WVO-vergunning A27. Report. Ministry of the Infrastructures and the Environment. Government of the Netherlands.

Brongers, I. (2011b). Jaarverslag 2011 monitoring WVO-vergunning A27. Report. Ministry of the Infrastructures and the Environment. Government of the Netherlands.

Climate data(a), (2018). Retrieved September, 14th, 2018, from https://www.climatedata.eu

Climate data(b) (2018). Retrieved September, 14th, 2018, from https://fr.climate-data.org

Coelho, P.M.D.H.S. (2009). Modelação matemática da qualidade da água em sistemas albufeira-rio. PhD Dissertation, NOVA School of Science and Technology, NOVA University of Lisbon. Retrieved from: https://run.unl.pt/handle/10362/2074

Crabtree, B., Dempsey, P., Moy, F., Brown, C., Song, M. (2008). Improved determination of pollutants in highway runoff. Stage 3 Report. United Kingdom Highways Agency.

Decree-Law no. 236/98, of 1 August of 1998. Official Gazette no. 176/1998, Series I-A of 1998-08-01. Lisbon: Ministry of the Environment of Portugal

Dempsey, P., & Song, M. (2008). Improved determination of pollutants in highway runoff. Stage 4 Report. United Kingdom Highways Agency.

EDF-DTG – Cemagref. (1993). Etude des Courbes Intensite-Duree-Frequence de Precipitations dans les Alpes. Rhône-Alpes.

El Dorado Weather (2018). Retrieved July, 15th, 2018 from https://eldoradoweather.com

Fernandes, J., Barbosa, A.E. (2018). WP 1 – Prediction of Pollutant Loads and Concentrations in Road Runoff. Task 1.1. Literature review on road runoff pollution on Europe. Deliverable Report from the PROPER project: Road Runoff Pollution management and mitigation of environmental risks. Lisbon: Conference of European Directors of Roads.

Gardiner, L.R., Moores, J., Osborne, A., Semadeni-Davies, A. (2016). Risk assessment of road stormwater runoff. New Zealand Transport Agency. Wellington, New Zealand: ARRB Group Ldt.

Google Earth (2018). Accessed from July to October of 2018 from https://www.google.com/earth/download/gep/agree.html

Granata, F., Gargano, R., De Marinis, G. (2016). Support Vector Regression for Rainfall-Runoff Modelling in Urban Drainage: A Comparison with the EPA's Storm Water Management Model. Water. 8(3), 69. https://doi.org/10.3390/w8030069

Granato, G. (2013a). Stochastic Empirical Loading and Dilution Model (SELDM) Version 1.0.0. U.S. Geological Survey Techniques and Methods, No. 4, Ch. C3, 112 pp. Retrieved from: http://pubs.usgs.gov/tm/04/c03/

Granato, G. (2013b). Stochastic Empirical Loading and Dilution Model (SELDM) Version 1.0.0 - Appendix 4, Navigating the graphical user interface. U.S. Geological Survey Techniques and Methods, No. 4, Ch.C3, 66 pp. Retrieved from: http://pubs.usgs.gov/tm/04/c03/

Granato, G.E. (2010). Methods for development of planning-level estimates of stormflow at unmonitored sites in the conterminous United States. Report. Federal Highway Administration. Washington: U.S. Department of Transportation.

Granato, G., Cazenas, P. (2009). Highway-runoff database (HRDB version 1.0): A data warehouse and pre-processor for the stochastic empirical loading and dilution model Report. Federal Highway Administration. Washington: U.S. Department of Transportation.

Granato, G., Jones, S. (2014). Estimating the risks for adverse effects of total phosphorus in receiving streams with the Stochastic Empirical Loading and Dilution Model (SELDM). Compendium of Papers for the Transportation Research Board 93rd Annual Meeting. Washington D.C., USA

Higgins, N. (2006). Analysis of highway runoff in Ireland. PhD Dissertation, Trinity College Dublin. Retrieved from: http://hdl.handle.net/2262/78421

Highways Agency. (2009). Highways Agency Water Risk Assessment Tool - Help guide. Help guide report. Version 1.0.

Hill, M.K. (2010). Understanding environmental pollution. 3rd Ed.. New York, USA: Cambridge University Press

Hvitved-Jacobsen, T., & Youssef, Y. (1991). Chapter 5 Highway runoff quality, environmental impacts and control. In Hamilton R.S., Harrison, R.M. (Eds.). Studies in Environmental Science (44, pp. 165-208). https://doi.org/10.1016/S0166-1116(08)70083-9

Irish, L., Lesso, W., Barrett, M., Malina, J., & Charbeneau, R. (1995). An evaluation of the factors affecting the quality of highway runoff in the Austin, Texas area. Report. Center for Research in Water Resources. The University of Texas at Austin .

Jotte, L., Raspati, G., & Azrague, K. (2017). Review of stormwater management practices. Klima 2050 Project Report (no. 7). SINTEF Building and Infrastructure.

Karlovits, G. (2010). Monte Carlo simulation to characterize runoff uncertainty in a changing climate. Master's Thesis, Washington State University. Retrieved from: http://www.dissertations.wsu.edu/Thesis/Fall2010/G_Karlovits_111710.pdf

Kayhanian, M., Fruchtman, B. D., Gulliver, J. S., Montanaro, C., Ranieri, E., & Wuertz, S. (2012). Review of highway runoff characteristics: Comparative analysis and universal implications. Water Research, 46(20), 6609–6624. https://doi.org/10.1016/j.watres.2012.07.026

Kayhanian, M., Suverkropp, C., Ruby, A., & Tsay, K. (2006). Characterization and prediction of highway runoff constituent event mean concentration. Journal of Environmental Management, 85, 279–295. https://doi.org/10.1016/j.jenvman.2006.09.024

Kobriger, N. P. and Geinopolos, A. (1984). Sources and migration of highway runoff pollutants. Vol III. Research Report. Federal Highway Administration. Washington D.C.

Korving, H., Noortwijk, J., Van Gelder, P., & Clemens, F. (2009). Risk-based design of sewer system rehabilitation. Structure and Infrastructure Engineering. 5(3). 215-227. https://doi.org/10.1080/15732470601114299

Krause, P., Boyle, D. P., & Bäse, F. (2005). Comparison of different efficiency criteria for hydrological model assessment. Advances in Geosciences. 5. 89–97 . https://doi.org/10.5194/adgeo-5-89-2005

Leitão, T., Barbosa, A.E., Henriques, M.J., Ikavalko, V.M., Menezes, J.T.M. (2005). Avaliação e Gestão Ambiental das Águas de Escorrências de Estradas. Final Report. Lisbon, Portugal: National Laboratory for Civil Engineering.

Lencastre, A., Franco, F.M. (2006). Lições de Hidrologia. 3rd edition. Lisbon, Portugal: Fundação FCT

Loague, K., & Corwin, D. L. (2005). Point and nonpoint source pollution. Encyclopedia of Hydrological Sciences, 1-13. John Wiley & Sons, Ltd. https://doi.org/10.1002/0470848944.hsa097

Maestri, B., Dorman, M., & Hartigan, J. (1988). Managing pollution from highway storm water runoff. Transportation Research Record, 1166, 5–21.

Met Éireann – The Irish meteorological service (2018). Retrieved May, 8th, 2018 from https://www.met.ie

Met office (2018). Retrieved September, 14th, 2018 from https://www.metoffice.gov.uk

Moy, F., & Crabtree, R. (2002a). Monitoring of pollution from highway runoff. A34-Gallos Brook. United Kingdom Highway Agency.

Moy, F., & Crabtree, R. (2002b). Monitoring of pollution from highway runoff. A34-River Enborne. United Kingdom Highway Agency.

Moy, F., & Crabtree, R. (2002c). Monitoring of pollution from highway runoff. A 417-River Frome. United Kingdom Highway Agency.

Moy, F., & Crabtree, R. (2002d). Monitoring of pollution from highway runoff. M4-Brinkworth Brook. United Kingdom Highway Agency.

Moy, F., & Crabtree, R. (2002e). Monitoring of pollution from highway runoff. M4-River Ray. United Kingdom Highway Agency.

Moy, F., & Crabtree, R. (2002f). Monitoring of pollution from highway runoff. M40-Souldern Brook. United Kingdom Highway Agency .

El Mufleh, A., Béchet, B., & Ruban, V. (2010). Study of trace metal-bearing phases in sediments from runoff water infiltration basins. Novatech 2010, Session 2.8. 1–10. Retrieved from: http://hdl.handle.net/2042/35846

Norwegian meteorological institute (2018). Retrieved May, 8th, 2018 from http://eklima.met.no

Official Journal of the European Community. Directive 2000/60/EC of the European parliament and of the council (2000). Retrieved June, 10th, 2018 from https://eur-lex.europa.eu

Piguet, P. (2007). Road runoff over the shoulder diffuse infiltration. Real-scale experimentation and optimization. PhD Dissertation, University of Lausanne. http://dx.doi.org/10.5075/epfl-thesis-3858

Portuguese environmental agency (2018). Portuguese hourly precipitation data. Retrieved May, 8th 2018 from https://snirh.apambiente.pt/

Ramana, G. V. (2014). Regression analysis of rainfall of runoff process of a typical watershed. International Journal of Science and Applied Information Technology, 3(1), 16–26. Retrieved from: http://warse.org/pdfs/2014/ijsait04312014.pdf

Ringler, S. (2007). First flush characterization of storm water runoff. Master's Thesis, University of New Orleans. Retrieved from: https://scholarworks.uno.edu/td/537

Road runoff pollution management and mitigation of environmental risks of the conference European directors of roads (2018). Retrieved July, 15th, 2018 from http://proper-cedr.eu

Royal Institute of Meteorology of the Netherlands (2018). Retrieved May, 8th, 2018 from https://www.knmi.nl/home

Santos, D. & Barbosa, A. E. (2004). Modelação da Qualidade das Águas de Escorrência de Estradas. 11.º Encontro Nacional de Saneamento Básico. Faro, Portugal.

Sitterson, J., Knightes, C., Parmar, R., Wolfe, K., Muche, M., & Avant, B. (2017). An overview of rainfall-runoff model types. United States Environmental Protection Agency. Washington DC, USA.

Solomon F. (2008). Environment and Communities: Impacts of Metals on Aquatic Ecosystems and Human Health. Mining.com, April 2008, 14–19.

Thornburg, T., & Lowe, J. (2009). Standard operating procedure for calculating pollutant loads for stormwater discharges. Olympia, WA, USA. Washington State Department of Ecology.

Transport Research Laboratory. (2002). Pollution from Roads and Vehicles and Dispersal to the Local Environment. Report. Project POLMIT (Pollution of Groundwater and Soil by Road and Traffic Sources: dispersal mechanisms, pathways and mitigation measures).

Trenouth, W.R. (2017). Highway Stormwater Runoff Quality: Investigation of Improved Operational, Predictive and Treatment Approaches. PhD Dissertation, University of Guelph. Retrieved from: http://hdl.handle.net/10214/10427

Trenouth, W.R., Gharabaghi, B. (2016). Highway runoff quality models for the protection of environmentally sensitive areas. Journal of Hydrology, 542, 143–155. https://doi.org/10.1016/j.jhydrol.2016.08.058

Vollertsen, J., Åstebøl, S., Coward, J., Fageraas, T., Madsen, H., Nielsen, A., & Hvitved-Jacobsen, T. (2007). Highway and urban environment: proceedings of the 8th highway and urban environment symposium. In G. Morrison & S. Rauch (Eds.), Highway and Urban Environment (pp. 499–509).

Weather and climate (2018). Retrieved May, 8th, 2018 http://www.meteofrance.com/accueil

Werner, I., Centre, S., Applied, F., Koger, C., Deanovic, L. A., & Hinton, D. E. (2001). Toxicity of methyl-tert-butyl-ether to freshwater organisms. Environmental Pollution. 83-88. https://doi.org/10.1016/S0269-7491(00)00027-0

Winkler, M. (2005). The characterization of highway runoff water quality. Master's Thesis, University of Graz. Retrieved from: http://lampx.tugraz.at/~portal/Files/i2150/download/Diplomarbeiten/DA_Winkler.pdf

World weather and climate information (2018). Retrieved September, 14th, 2018 from https://weather-and-climate.com

Yannopoulos, S., Basbas, S., & Giannopoulou, I. (2013). Water bodies pollution due to highways stormwater runoff: Measures and legislative framework. Global Nest Journal, 15(1), 85–92.

Annexes

Annex I – Monitored EMC of each studied highway

Highways	Code	TSS (mg/L)	Cu (μg/L)	Zn (μg/L)	Pb (μg/L)	Cd (μg/L)	Fe (mg/L)	Cr (μg/L)
A 1	P1	26,200	32,907	276,984	9,000	0,136	0,200	ND
		15,600	20,758	157,625	4,176	0,099	1,900	15,283
		10,300	7,506	73,422	ND	0,059	0,100	ND
		13,800	13,883	92,633	ND	0,048	0,121	0,762
		9,800	13,732	59,899	ND	0,154	0,036	ND
		1,200	10,815	21,078	ND	0,055	0,092	0,477
		100,800	23,540	153,338	3,771	0,095	0,472	0,743
		7,000	30,766	135,082	2,785	0,102	0,005	ND
		36,000	21,713	189,094	5,645	0,073	0,600	ND
		8,900	16,783	81,536	0,914	0,095	0,122	0,312
A 2	P2	5,000	5,400	40,000	ND	ND	0,100	ND
		2,400	14,000	70,000	0,100	ND	0,120	ND
		0,097	14,000	97,000	4,100	ND	0,110	ND
A 6	P3	1,600	2,400	217,000	1,000	ND	0,118	ND
		6,700	9,100	1443,000	1,000	ND	0,211	ND
		3,200	4,800	46,000	1,000	ND	0,080	ND
		60,300	14,000	168,000	4,700	ND	0,672	ND
		19,100	11,000	104,000	1,000	ND	0,766	ND
		27,000	7,300	97,000	2,300	ND	0,273	ND
A 22	P4	40,600	30,000	ND	10,000	ND	2,400	ND
		50,000	30,000	ND	20,000	ND	2,800	ND
		82,400	20,000	ND	20,000	ND	2,200	ND
		88,000	20,000	ND	20,000	ND	1,800	ND
		79,500	30,000	ND	30,000	ND	3,300	ND
		32,100	20,000	ND	20,000	ND	1,200	ND
		47,900	20,000	ND	30,000	ND	2,100	ND
		25,700	20,000	ND	30,000	ND	0,900	ND
		25,800	30,000	ND	30,000	ND	0,700	ND
A 25	P5	26,600	63,600	133,190	28,700	ND	1,269	ND
		101,000	73,000	234,960	55,500	ND	2,723	ND
		47,700	58,900	162,980	35,700	ND	1,855	ND
		28,900	35,500	81,000	33,000	ND	0,898	ND
		43,600	84,300	81,690	43,100	ND	1,909	ND
		96,700	76,600	134,070	41,700	ND	3,712	ND
		159,600	175,900	406,850	69,700	ND	7,352	ND
		31,200	47,400	96,410	20,000	ND	1,600	ND
		109,400	86,100	200,910	49,100	ND	4,972	ND
		78,200	38,800	94,690	66,400	ND	2,653	ND
		96,000	38,800	139,280	21,800	ND	1,997	ND
		207,300	88,000	252,320	35,600	ND	4,882	ND

Highways	Code	TSS (mg/L)	Cu (µg/L)	Zn (µg/L)	Pb (µg/L)	Cd (µg/L)	Fe (mg/L)	Cr (µg/L)
A 25	P5	139,500	75,000	213,800	25,900	ND	3,001	ND
		25,700	32,000	82,620	18,000	ND	0,748	ND
		16,100	22,400	81,760	18,000	ND	0,774	ND
		87,500	655,800	274,660	46,200	ND	1,307	ND
		31,200	47,900	126,000	18,000	ND	1,230	ND
		9,200	5,500	30,220	6,500	ND	0,195	ND
		53,400	49,800	153,270	20,300	ND	2,400	ND
		17,400	23,700	88,680	18,000	ND	0,701	ND
		30,700	217,500	122,290	21,900	ND	0,695	ND
		52,000	70,400	127,360	18,000	ND	1,322	ND
		32,100	79,900	102,980	18,000	ND	0,653	ND
		20,300	57,800	88,630	18,000	ND	0,774	ND
		50,000	134,800	145,610	18,000	ND	1,376	ND
		8,600	44,900	88,440	18,000	ND	0,315	ND
		2,200	10,500	81,310	18,000	ND	0,035	ND
		15,400	33,800	81,250	18,000	ND	0,120	ND
		45,000	78,300	168,360	18,000	ND	2,414	ND
		75,500	99,000	115,180	22,400	ND	1,859	ND
IP 6	P6	365,399	69,844	147,121	11,865	1,429	ND	9,500
		191,292	43,455	85,091	2,455	1,000	ND	3,000
		23,804	30,565	17,529	23,413	1,000	ND	3,000
		214,455	31,841	55,098	3,841	1,000	ND	3,000
		509,973	46,459	106,622	14,581	1,000	ND	16,973
		60,011	19,123	86,476	1,987	ND	ND	ND
		241,500	7,351	48,350	2,235	ND	ND	ND
		50,218	3,000	39,102	1,000	ND	ND	ND
A 27 - pervious	N1	ND	180,000	1300,000	52,000	2,000	ND	21,000
		ND	88,000	250,000	15,000	1,000	ND	19,000
		ND	11,000	31,000	8,000	2,000	ND	10,000
		ND	15,000	220,000	5,000	1,000	ND	52,000
		ND	420,000	1900,000	130,000	2,000	ND	19,000
		ND	73,000	230,000	13,000	ND	ND	ND
		ND	16,000	59,000	6,000	ND	ND	ND
		ND	ND	17,000	10,000	ND	ND	ND
A 27 - Impervious	N2	ND	31,000	130,000	17,000	1,000	ND	14,000
		ND	17,000	54,000	14,000	1,000	ND	10,000
		ND	21,000	60,000	9,000	1,000	ND	10,000
		ND	30,000	160,000	12,000	1,000	ND	10,000
		ND	77,000	270,000	27,000	1,000	ND	29,000
		ND	11,000	92,000	11,000	1,000	ND	10,000
		ND	17,000	66,000	11,000	1,000	ND	12,000
E 6	N3	99,000	73,000	155,000	5,600	0,080	ND	ND
		181,000	74,200	241,000	12,000	0,130	ND	ND

Highways	**Code**	**TSS (mg/L)**	**Cu (µg/L)**	**Zn (µg/L)**	**Pb (µg/L)**	**Cd (µg/L)**	**Fe (mg/L)**	**Cr (µg/L)**
E 6	N3	388,000	118,000	391,000	29,000	0,340	ND	ND
		522,000	129,000	380,000	28,000	0,350	ND	ND
		96,000	48,600	110,000	8,900	0,120	ND	ND
		107,000	37,300	67,900	1,700	ND	ND	ND
		425,000	133,000	319,000	25,000	0,210	ND	ND
		115,000	25,400	66,800	9,400	0,080	ND	ND
		401,000	84,000	285,000	24,000	0,230	ND	ND
		171,000	60,800	63,300	1,500	ND	ND	ND
		128,000	48,600	175,000	8,600	0,100	ND	ND
		182,000	114,000	189,000	10,000	0,060	ND	ND
		91,000	84,300	124,000	8,900	0,120	ND	ND
		184,000	130,000	96,500	7,600	1,000	ND	ND
		78,000	85,100	140,000	10,000	0,100	ND	ND
		93,000	66,800	149,000	10,000	0,110	ND	ND
		48,000	90,700	128,000	9,800	0,070	ND	ND
		240,000	92,000	323,000	23,000	0,280	ND	ND
		344,000	103,000	371,000	27,000	0,300	ND	ND
		430,000	102,000	408,000	26,000	0,290	ND	ND
		259,000	61,100	235,000	19,000	0,150	ND	ND
		275,000	94,000	266,000	16,000	0,230	ND	ND
		159,000	77,000	211,000	8,400	0,200	ND	ND
		295,000	112,000	355,000	19,000	0,240	ND	ND
		606,000	118,000	544,000	33,000	0,350	ND	ND
		39,000	41,400	66,900	4,200	0,060	ND	ND
		201,000	72,600	170,000	10,000	0,080	ND	ND
		216,000	78,600	266,000	16,000	0,190	ND	ND
A 11 – pervious	F1	65,900	49,000	284,000	60,600	0,610	ND	ND
		94,000	92,500	613,000	92,900	1,010	ND	ND
		47,400	31,200	245,000	28,400	0,490	ND	ND
		46,700	32,400	240,000	27,600	1,640	ND	ND
		36,100	73,700	254,000	33,600	0,630	ND	ND
		61,300	42,600	238,000	49,400	1,600	ND	ND
		31,300	31,400	145,000	35,600	0,470	ND	ND
		27,300	14,300	104,000	21,200	0,460	ND	ND
		117,000	48,000	392,000	70,500	0,740	ND	ND
		25,100	56,600	434,000	21,100	0,370	ND	ND
		32,000	89,700	659,000	43,000	1,870	ND	ND
		220,000	94,200	805,000	126,000	1,030	ND	ND
		238,000	80,000	615,000	138,000	2,130	ND	ND
		20,100	24,800	143,000	21,700	0,510	ND	ND
		24,400	45,800	269,000	17,000	0,860	ND	ND
		20,700	21,600	212,000	18,000	0,280	ND	ND
		92,500	40,500	263,000	62,000	1,020	ND	ND

Highways	Code	TSS (mg/L)	Cu (µg/L)	Zn (µg/L)	Pb (µg/L)	Cd (µg/L)	Fe (mg/L)	Cr (µg/L)
A 11 - pervious	F1	70,000	146,000	709,000	53,000	1,260	ND	ND
		78,300	42,300	380,000	46,200	0,430	ND	ND
		20,700	35,700	131,000	18,600	0,440	ND	ND
		37,500	27,200	163,000	37,400	0,800	ND	ND
		34,300	22,900	166,000	25,000	1,310	ND	ND
		30,200	26,400	145,000	26,100	0,470	ND	ND
		24,600	25,400	126,000	23,400	0,330	ND	ND
		33,200	23,300	152,000	21,100	0,380	ND	ND
		42,000	24,500	124,000	32,900	0,230	ND	ND
		16,300	50,600	415,000	20,100	1,170	ND	ND
		21,500	28,400	248,000	29,800	0,370	ND	ND
		27,000	31,000	174,000	23,900	0,360	ND	ND
		29,000	11,200	120,000	13,700	0,790	ND	ND
		35,600	25,100	133,000	39,600	0,370	ND	ND
		43,200	28,700	311,000	61,400	2,790	ND	ND
		56,900	31,000	236,000	66,000	1,610	ND	ND
		44,100	27,100	228,000	56,600	0,210	ND	ND
		31,900	31,400	197,000	45,300	0,420	ND	ND
		143,000	36,700	618,000	156,000	1,200	ND	ND
		180,000	83,700	576,000	155,000	1,850	ND	ND
		83,400	39,400	274,000	67,600	0,510	ND	ND
		44,600	24,000	181,000	33,200	0,390	ND	ND
		67,100	29,500	268,000	42,000	1,350	ND	ND
		59,300	26,200	174,000	46,900	2,420	ND	ND
		267,000	63,100	408,000	180,000	0,550	ND	ND
		138,000	73,400	527,000	118,000	1,000	ND	ND
		113,000	73,100	269,000	93,500	0,520	ND	ND
		71,000	32,900	1544,000	44,200	1,680	ND	ND
		125,000	69,000	554,000	95,900	0,450	ND	ND
		70,400	46,900	465,000	71,800	1,240	ND	ND
		211,000	98,600	1322,000	188,000	4,160	ND	ND
		48,500	27,000	195,000	39,600	3,760	ND	ND
A 11 – impervious	F2	3,900	16,900	131,000	3,900	0,340	ND	ND
		48,100	106,400	352,000	33,000	0,150	ND	ND
		14,400	41,500	246,000	10,300	0,120	ND	ND
		22,800	24,500	121,000	17,900	0,040	ND	ND
		10,500	21,500	83,000	8,600	0,140	ND	ND
		63,100	30,300	227,000	19,500	0,230	ND	ND
		8,300	14,100	99,000	8,300	0,120	ND	ND
		5,600	15,500	67,000	7,700	0,050	ND	ND
		4,100	ND	66,000	3,800	0,190	ND	ND
		4,400	11,700	56,000	4,800	0,110	ND	ND
		52,700	150,100	368,000	60,800	0,190	ND	ND

Highways	Code	TSS (mg/L)	Cu (µg/L)	Zn (µg/L)	Pb (µg/L)	Cd (µg/L)	Fe (mg/L)	Cr (µg/L)
A 11 – impervious	F2	33,800	98,300	198,000	24,900	1,890	ND	ND
		12,600	48,600	130,000	31,200	0,160	ND	ND
		9,900	46,200	134,000	10,100	0,090	ND	ND
		8,100	19,400	80,000	6,200	0,160	ND	ND
		2,700	9,500	44,000	2,200	0,040	ND	ND
		17,000	72,200	183,000	12,800	0,160	ND	ND
		7,700	42,400	133,000	21,000	0,150	ND	ND
		4,200	31,400	110,000	8,300	0,160	ND	ND
		6,000	18,100	50,000	6,900	1,070	ND	ND
		5,500	22,100	63,000	6,800	0,600	ND	ND
		9,700	16,900	51,000	6,700	0,300	ND	ND
		5,900	16,100	78,000	9,300	0,100	ND	ND
		6,900	31,400	125,000	8,800	0,410	ND	ND
		7,700	16,100	65,000	8,500	0,150	ND	ND
		5,700	4,900	44,000	5,100	0,250	ND	ND
		2,300	6,100	58,000	6,500	0,420	ND	ND
		5,000	19,600	86,000	9,500	1,110	ND	ND
		6,900	15,100	78,000	12,300	0,110	ND	ND
		2,400	8,700	98,000	11,700	0,170	ND	ND
		8,900	13,200	89,000	8,100	1,460	ND	ND
		6,200	9,600	67,000	6,700	0,430	ND	ND
		4,500	11,700	110,000	11,700	0,480	ND	ND
		8,000	33,800	631,000	9,900	2,400	ND	ND
		12,700	12,600	93,000	12,000	0,290	ND	ND
		36,900	30,900	633,000	24,900	1,810	ND	ND
		4,400	18,100	410,000	6,000	1,030	ND	ND
		16,500	11,800	133,000	13,800	0,790	ND	ND
		11,400	18,800	128,000	13,500	1,370	ND	ND
		4,100	7,800	42,000	7,200	0,110	ND	ND
		5,100	6,000	48,000	2,000	0,110	ND	ND
		8,400	70,200	1096,000	39,200	0,950	ND	ND
		13,100	31,000	195,000	15,300	0,330	ND	ND
		6,400	21,300	172,000	13,300	0,250	ND	ND
		8,900	52,800	280,000	15,100	0,120	ND	ND
		7,700	22,860	88,000	6,600	0,120	ND	ND
		7,900	12,040	76,000	3,700	0,240	ND	ND
		3,700	9,250	76,000	2,900	0,210	ND	ND
		3,300	15,780	99,000	2,800	0,740	ND	ND
		2,300	11,810	96,000	3,200	0,230	ND	ND
		4,600	9,250	70,000	3,600	0,090	ND	ND
		2,300	9,250	96,000	3,000	0,210	ND	ND
		5,800	25,240	138,000	10,200	0,200	ND	ND
		5,700	9,900	153,000	4,800	0,050	ND	ND

Highways	Code	TSS (mg/L)	Cu (µg/L)	Zn (µg/L)	Pb (µg/L)	Cd (µg/L)	Fe (mg/L)	Cr (µg/L)
A 11 – impervious	F2	2,000	< 2	160,000	13,200	0,300	ND	ND
M 7 - Kildare	I1	2340,000	207,000	969,000	222,000	18,900	ND	ND
		256,000	39,700	109,000	21,100	4,270	ND	ND
		1350,000	140,000	550,000	156,000	9,000	ND	ND
		519,000	70,800	272,000	59,000	5,000	ND	ND
		181,000	62,000	295,000	43,700	8,290	ND	ND
		208,000	41,300	147,000	14,800	9,000	ND	ND
		ND	89,900	445,000	87,900	10,000	ND	ND
		368,000	94,900	521,000	63,300	9,540	ND	ND
		476,000	ND	ND	ND	ND	ND	ND
		404,000	95,500	554,000	116,000	6,300	ND	ND
		1720,000	259,000	1520,000	319,000	12,200	ND	ND
		704,000	152,000	956,000	188,000	9,160	ND	ND
		2210,000	293,000	1750,000	373,000	8,430	ND	ND
		302,000	77,800	407,000	97,300	5,500	ND	ND
		433,000	73,100	457,000	115,000	0,660	ND	ND
		2020,000	230,000	1400,000	274,000	16,100	ND	ND
		430,000	74,400	393,000	106,000	8,120	ND	ND
		125,000	47,900	205,000	75,800	6,110	ND	ND
		1370,000	171,000	1050,000	177,000	10,000	ND	ND
M 7 - Monasterevin	I2	163,000	59,100	218,000	86,900	6,170	ND	ND
		116,000	41,600	146,000	59,800	2,660	ND	ND
		60,900	43,400	151,000	63,100	5,760	ND	ND
		154,000	40,900	239,000	74,600	5,740	ND	ND
		258,000	69,100	318,000	79,200	7,070	ND	ND
		127,000	42,300	210,000	72,300	2,820	ND	ND
		184,000	51,700	166,000	64,900	5,120	ND	ND
		183,000	43,500	138,000	50,500	3,510	ND	ND
M 7 - Portlaoise	I3	25,400	23,000	106,000	87,000	9,400	ND	ND
		44,400	43,000	32,000	89,000	4,000	ND	ND
		59,800	6,000	18,000	79,000	2,000	ND	ND
		116,000	26,200	154,000	59,400	7,230	ND	ND
		14,500	33,000	150,000	95,000	24,000	ND	ND
		37,000	17,000	32,000	52,000	5,000	ND	ND
M 4 – Brinkworth	E1	235,670	67,000	246,000	ND	ND	ND	ND
		41,230	29,000	160,000	ND	ND	ND	ND
		246,500	13,000	84,000	ND	ND	ND	ND
		29,230	ND	32,000	ND	ND	ND	ND
		47,610	25,000	81,000	ND	ND	ND	ND
		21,770	31,000	85,000	ND	ND	ND	ND
		96,460	28,000	54,000	ND	ND	ND	ND
		15,150	23,000	94,000	ND	ND	ND	ND

Highways	Code	TSS (mg/L)	Cu (µg/L)	Zn (µg/L)	Pb (µg/L)	Cd (µg/L)	Fe (mg/L)	Cr (µg/L)
M 4 - Brinkworth	E1	87,940	ND	66,000	ND	ND	ND	ND
		64,480	24,000	105,000	ND	ND	ND	ND
M 4 - River Ray	E2	124,740	33,000	115,000	60,000	ND	ND	ND
		89,000	17,000	56,000	ND	ND	ND	ND
		663,000	16,000	294,000	ND	ND	ND	ND
		86,000	15,000	51,000	ND	ND	ND	ND
		62,000	13,000	90,000	ND	ND	ND	ND
		384,000	242,000	688,000	178,000	0,960	ND	49,900
		95,000	39,900	250,000	23,400	5,400	ND	3,300
		1350,000	36,400	143,000	29,500	0,800	ND	5,700
		193,000	93,400	384,000	88,800	1,300	ND	21,100
		62,000	40,400	144,000	34,200	0,400	ND	9,600
M 40	E3	45,960	26,800	94,400	5,860	0,540	ND	3,100
		53,360	26,100	81,900	9,290	0,340	ND	4,600
		60,560	93,800	316,000	27,800	0,740	ND	9,300
		61,020	37,100	108,000	13,300	0,500	ND	2,100
		ND	35,200	140,000	16,200	0,340	ND	4,500
		31,880	22,000	21,100	4,830	0,140	ND	6,700
		29,270	20,900	68,700	6,520	0,240	ND	1,900
		30,580	35,600	123,000	12,000	0,350	ND	2,800
		87,410	86,300	379,000	36,000	0,790	ND	9,500
		57,850	42,700	161,000	19,800	0,360	ND	3,700
A 417	E4	44,400	25,400	72,200	4,500	0,290	ND	4,300
		44,900	49,700	45,200	0,200	0,100	ND	2,900
		32,800	15,400	53,600	5,200	0,230	ND	2,500
		21,900	16,600	61,900	6,600	0,220	ND	4,300
		82,900	10,200	41,700	6,300	0,100	ND	1,700
		45,200	32,800	52,400	3,610	0,170	ND	2,600
		16,300	23,200	55,700	3,290	0,120	ND	0,900
		54,100	30,400	69,100	5,650	0,240	ND	3,400
		120,300	22,700	53,700	7,440	0,190	ND	2,800
		184,800	13,500	20,500	1,000	0,400	ND	1,800
A 34 - Gallos Brook	E5	181,940	108,000	390,000	88,900	ND	ND	12,000
		27,770	31,500	140,000	15,200	0,190	ND	4,640
		99,500	79,400	207,000	61,500	1,000	ND	15,800
		37,710	42,600	73,700	21,800	0,580	ND	5,900
		20,310	20,200	41,000	3,500	0,160	ND	5,900
		18,420	24,900	48,600	8,100	0,160	ND	6,000
		135,130	82,600	291,000	46,800	0,910	ND	6,600
		231,000	83,000	329,000	63,800	0,820	ND	6,500
		179,000	104,000	397,000	95,900	1,110	ND	13,200
		80,550	103,000	280,000	99,000	0,620	ND	14,300
		129,920	13,000	60,000	2,000	0,400	ND	3,800

Highways	Code	TSS (mg/L)	Cu (µg/L)	Zn (µg/L)	Pb (µg/L)	Cd (µg/L)	Fe (mg/L)	Cr (µg/L)
A 34 - River Enborne	E6	38,510	63,500	30,400	39,100	0,640	ND	8,800
		114,950	27,100	15,800	12,600	0,130	ND	3,200
		66,210	75,900	46,000	48,400	0,370	ND	13,400
		136,560	24,500	8,500	13,000	0,280	ND	2,900
		73,550	49,900	26,000	33,500	0,220	ND	4,400
		130,180	23,500	14,900	3,570	0,090	ND	2,700
		50,800	15,500	38,700	2,040	0,100	ND	30,000
		40,010	11,000	20,500	4,810	0,130	ND	6,600
		46,280	20,700	29,300	6,710	0,160	ND	1,500

*ND means no monitored data available

Annex II - SELDM GUI

This chapter presents the graphical user interface of the SELDM, which can be reviewed in more detail in the fourth annex of SELDM's help guide (Granato, 2013c). In this demonstration, only one image of each form was shown, in order to give the idea of how the SELDM inputs work. Every sub-form that has a direct influence in the results of this work is presented.

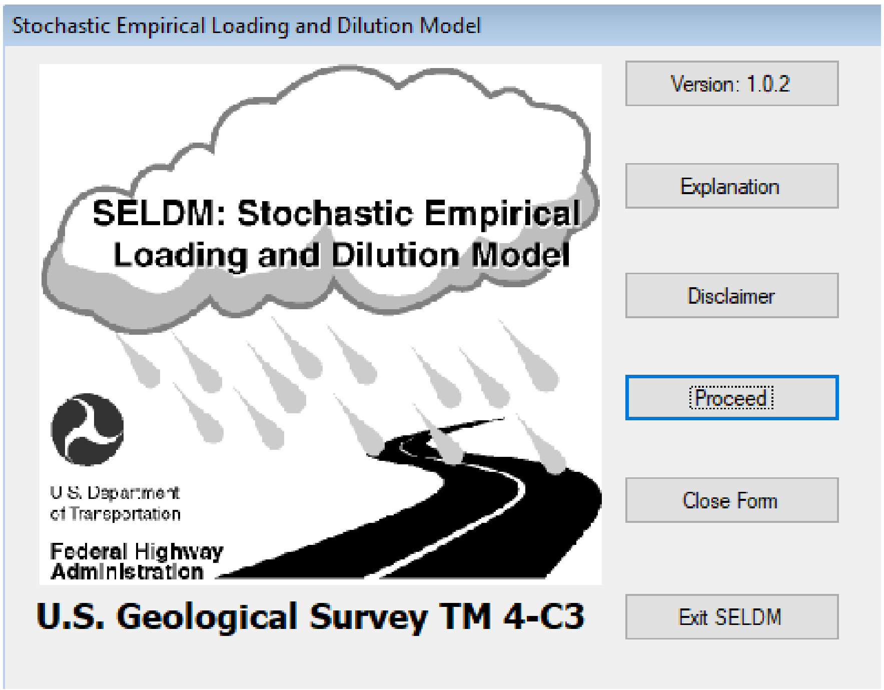
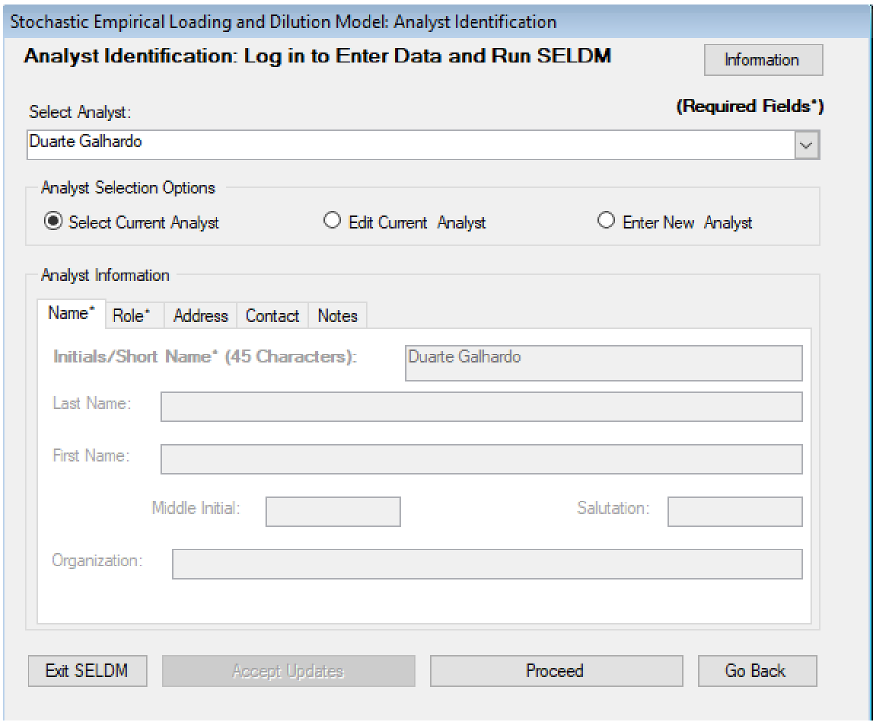


Figure II.1 – Opening form.

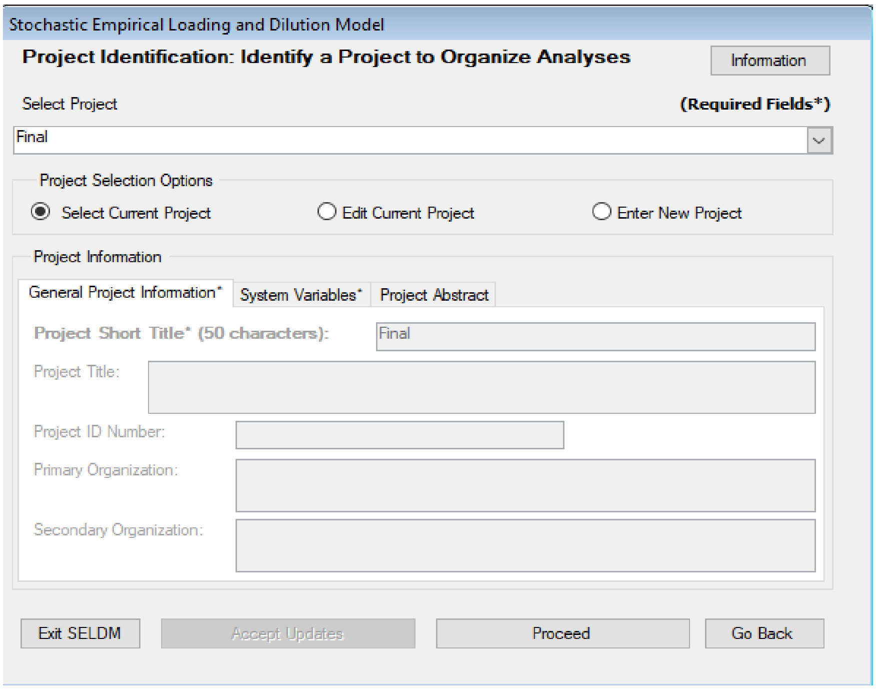


Select Analyst: Duarte Galhardo

● Select Current Analyst ○ Edit Current Analyst ○ Enter New Analyst

Initials/Short Name* (45 Characters): Duarte Galhardo

Figure II.2 – Analysis identification form. In this form there are five forms to be fulfilled.

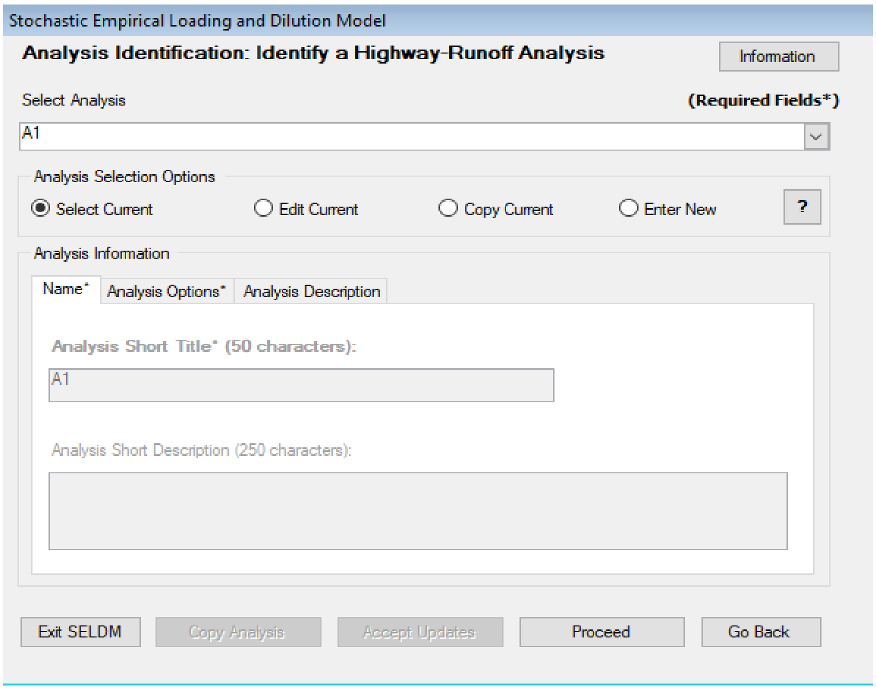


Select Project: Final

● Select Current Project ○ Edit Current Project ○ Enter New Project

Project Short Title* (50 characters): Final

Figure II.3 – Project identification form. Form to fill with the project information including two more tabs (System variables and project abstract).



Stochastic Empirical Loading and Dilution Model

Analysis Identification: Identify a Highway-Runoff Analysis

(Required Fields*)

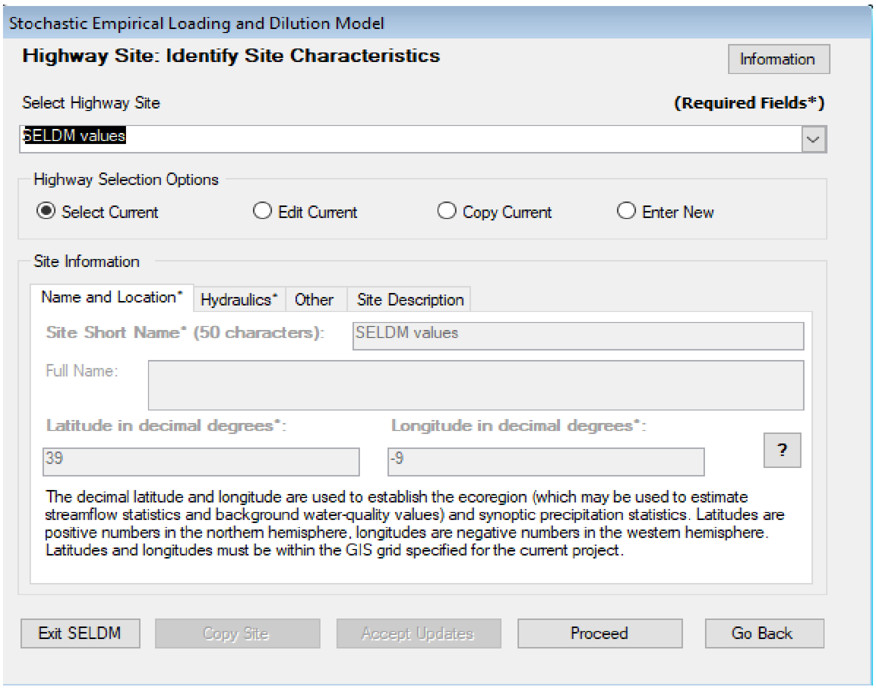
Select Analysis: A1

● Select Current ○ Edit Current ○ Copy Current ○ Enter New

Analysis Short Title* (50 characters): A1

Analysis Short Description (250 characters):

Figure II.4 – Analysis identification form. Form that allows the user to identify the road under study.



Stochastic Empirical Loading and Dilution Model

Highway Site: Identify Site Characteristics

(Required Fields*)

Select Highway Site: SELDM values

● Select Current ○ Edit Current ○ Copy Current ○ Enter New

Site Short Name* (50 characters): SELDM values

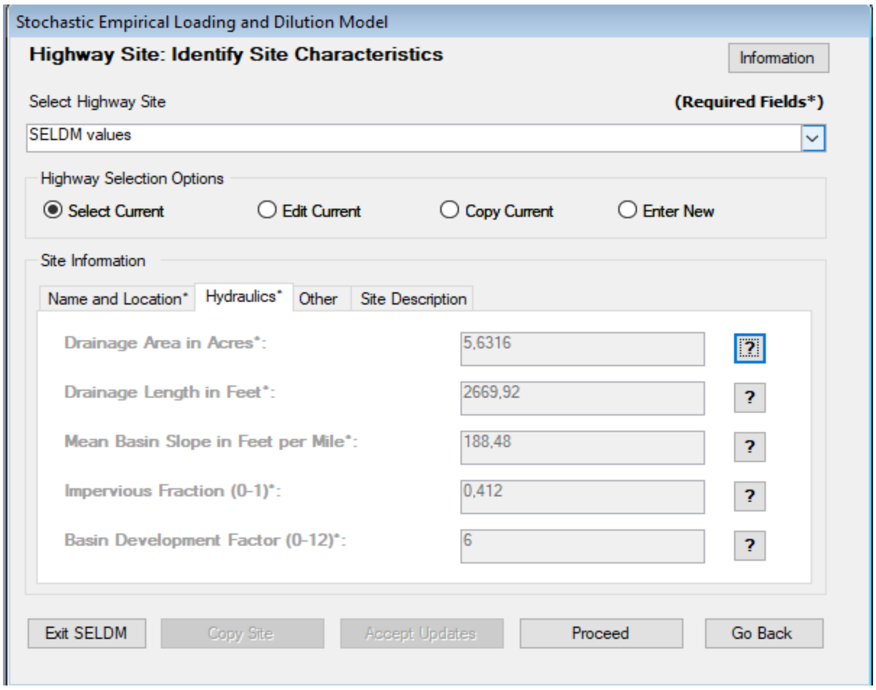
Full Name:

Latitude in decimal degrees*: 39

Longitude in decimal degrees*: -9

The decimal latitude and longitude are used to establish the ecoregion (which may be used to estimate streamflow statistics and background water-quality values) and synoptic precipitation statistics. Latitudes are positive numbers in the northern hemisphere, longitudes are negative numbers in the western hemisphere. Latitudes and longitudes must be within the GIS grid specified for the current project.

Figure II.5 – Highway site form – first tab . This is the first form that is important for the results presented in this work. In the first tab, it is mandatory to fil the location, in order for the model to have the information if the studied site is in the USA (and calculate precipitation statistics automatically) or not (in this case, it is mandatory to fil the precipitation statistics form).



Highway Site: Identify Site Characteristics

(Required Fields*)

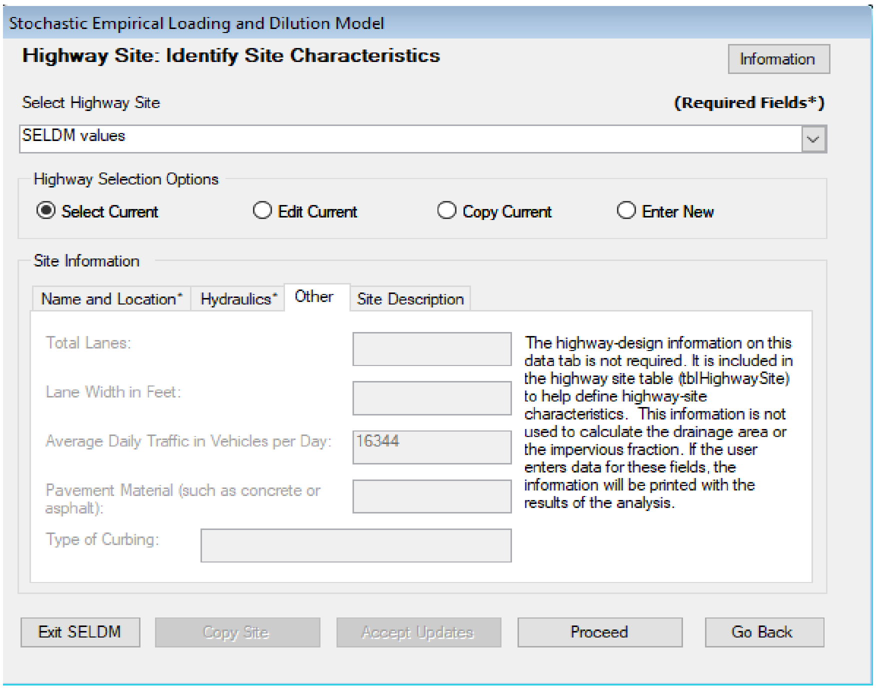
Select Highway Site: SELDM values

Highway Selection Options: ● Select Current ○ Edit Current ○ Copy Current ○ Enter New

Site Information: Name and Location* | Hydraulics* | Other | Site Description

Drainage Area in Acres*:	5,6316
Drainage Length in Feet*:	2669,92
Mean Basin Slope in Feet per Mile*:	188,48
Impervious Fraction (0-1)*:	0,412
Basin Development Factor (0-12)*:	6

Figure II.6 – Highway site form – second tab. The second tab of the highway site form concerns to the physical characteristics of the road studied.



Highway Site: Identify Site Characteristics

(Required Fields*)

Select Highway Site: SELDM values

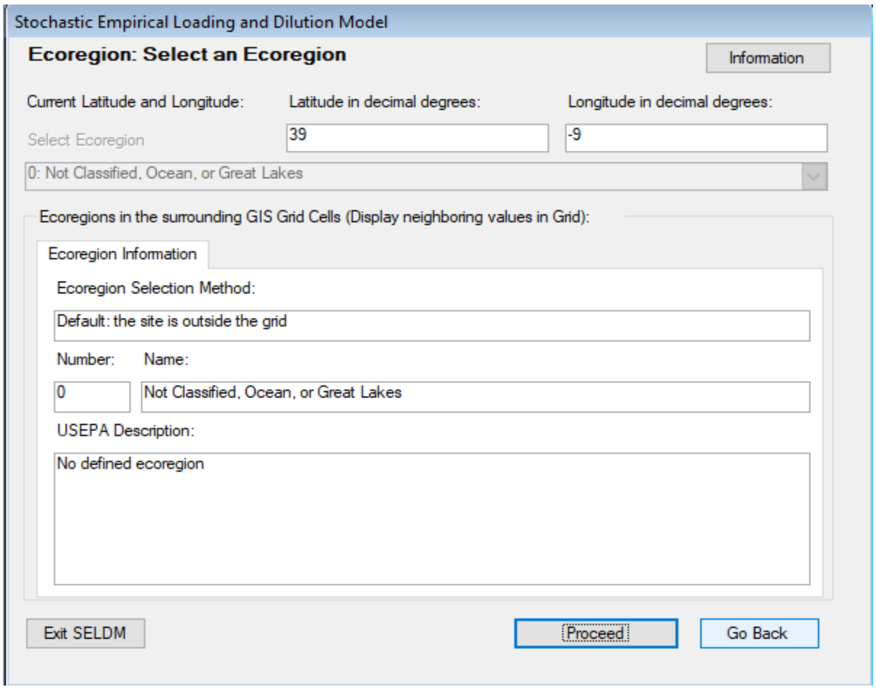
Highway Selection Options: ● Select Current ○ Edit Current ○ Copy Current ○ Enter New

Site Information: Name and Location* | Hydraulics* | Other | Site Description

Total Lanes:	
Lane Width in Feet:	
Average Daily Traffic in Vehicles per Day:	16344
Pavement Material (such as concrete or asphalt):	
Type of Curbing:	

The highway-design information on this data tab is not required. It is included in the highway site table (tblHighwaySite) to help define highway-site characteristics. This information is not used to calculate the drainage area or the impervious fraction. If the user enters data for these fields, the information will be printed with the results of the analysis.

Figure II.7 – Highway site form – third tab. The third tab of the highway site form concerns to other information of the road that is not required to run the model but it serves to better define the highway site.



Ecoregion: Select an Ecoregion

Current Latitude and Longitude:

Latitude in decimal degrees: 39

Longitude in decimal degrees: -9

Select Ecoregion: 0: Not Classified, Ocean, or Great Lakes

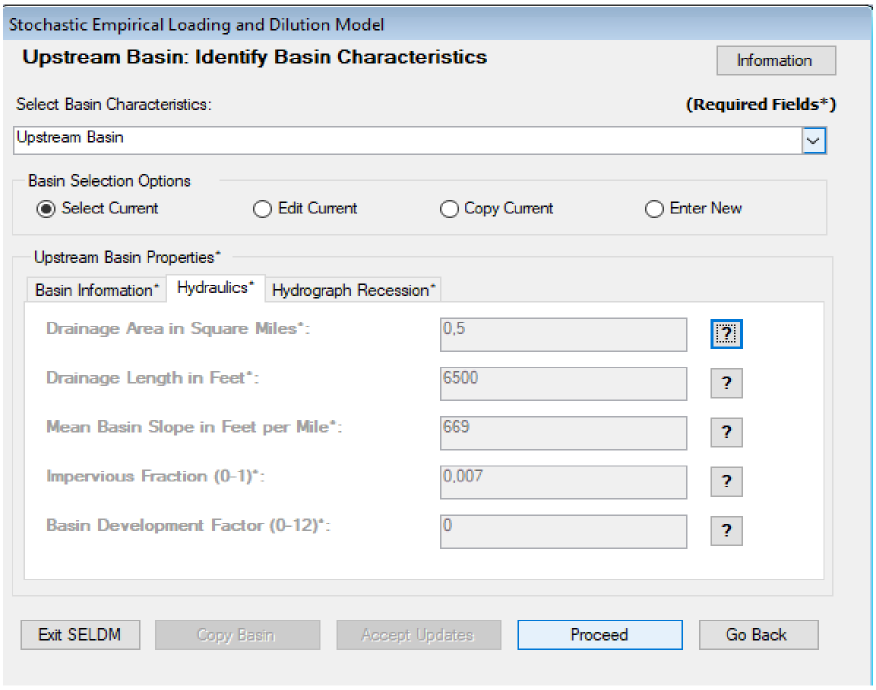
Ecoregion Selection Method: Default: the site is outside the grid

Number: 0

Name: Not Classified, Ocean, or Great Lakes

USEPA Description: No defined ecoregion

Figure II.8 – Ecoregion form. This form, in this study was always “Not classified”, because this region is only defined in the USA. With the definition of this region (through the coordinates in the first tab of the highway site form) the model automatically calculates the precipitation pattern



Upstream Basin: Identify Basin Characteristics

Select Basin Characteristics: **(Required Fields*)**

Upstream Basin

● Select Current ○ Edit Current ○ Copy Current ○ Enter New

Drainage Area in Square Miles*: 0,5

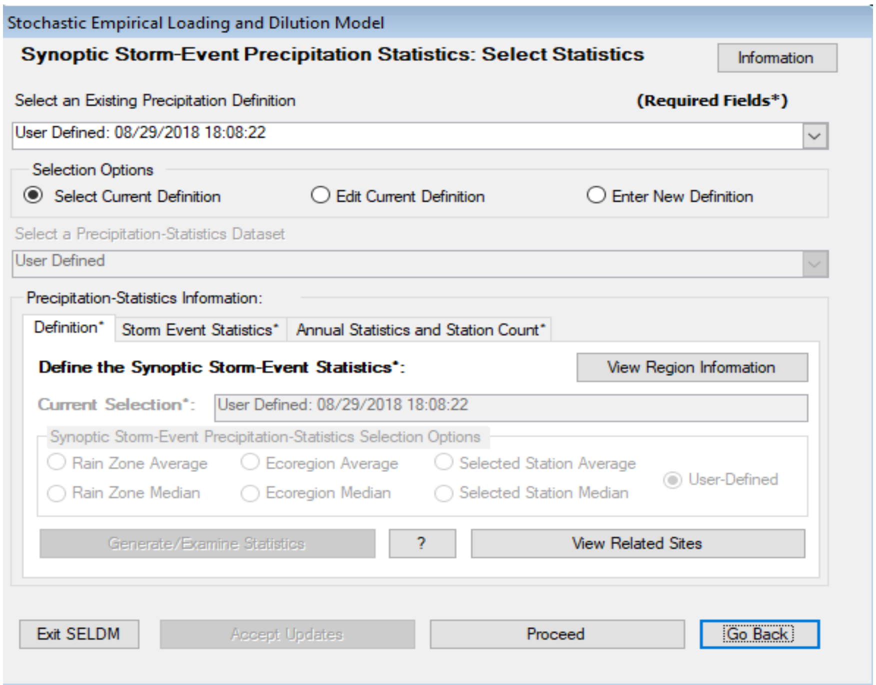
Drainage Length in Feet*: 6500

Mean Basin Slope in Feet per Mile*: 669

Impervious Fraction (0-1)*: 0,007

Basin Development Factor (0-12)*: 0

Figure II.9 – Upstream basin with hydraulics characteristics form. There are two other tabs in order to fill with basin information and hydrograph recession


Stochastic Empirical Loading and Dilution Model

Synoptic Storm-Event Precipitation Statistics: Select Statistics

Select an Existing Precipitation Definition **(Required Fields*)**

User Defined: 08/29/2018 18:08:22

Selection Options

● Select Current Definition ○ Edit Current Definition ○ Enter New Definition

Select a Precipitation-Statistics Dataset

User Defined

Precipitation-Statistics Information:

Definition* | Storm Event Statistics* | Annual Statistics and Station Count*

Define the Synoptic Storm-Event Statistics*:

Current Selection*: User Defined: 08/29/2018 18:08:22

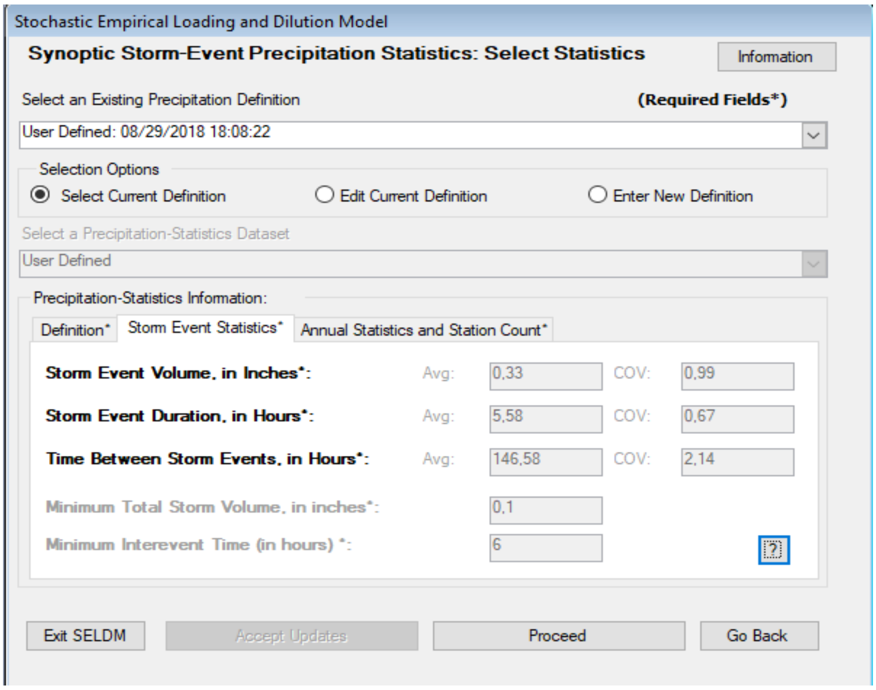
Synoptic Storm-Event Precipitation-Statistics Selection Options

○ Rain Zone Average ○ Ecoregion Average ○ Selected Station Average

○ Rain Zone Median ○ Ecoregion Median ○ Selected Station Median

● User-Defined

Figure II.10 – Synoptic storm-event Precipitation statistics form – first tab. The second form that influences the results studied in this work is synoptic storm-event precipitation statistics form. In the first tab, it is intended that the user chooses the option to calculate the precipitation statistics. In this case, the user-defined option is the only option.


Stochastic Empirical Loading and Dilution Model

Synoptic Storm-Event Precipitation Statistics: Select Statistics

Select an Existing Precipitation Definition **(Required Fields*)**

User Defined: 08/29/2018 18:08:22

Selection Options

● Select Current Definition ○ Edit Current Definition ○ Enter New Definition

Select a Precipitation-Statistics Dataset

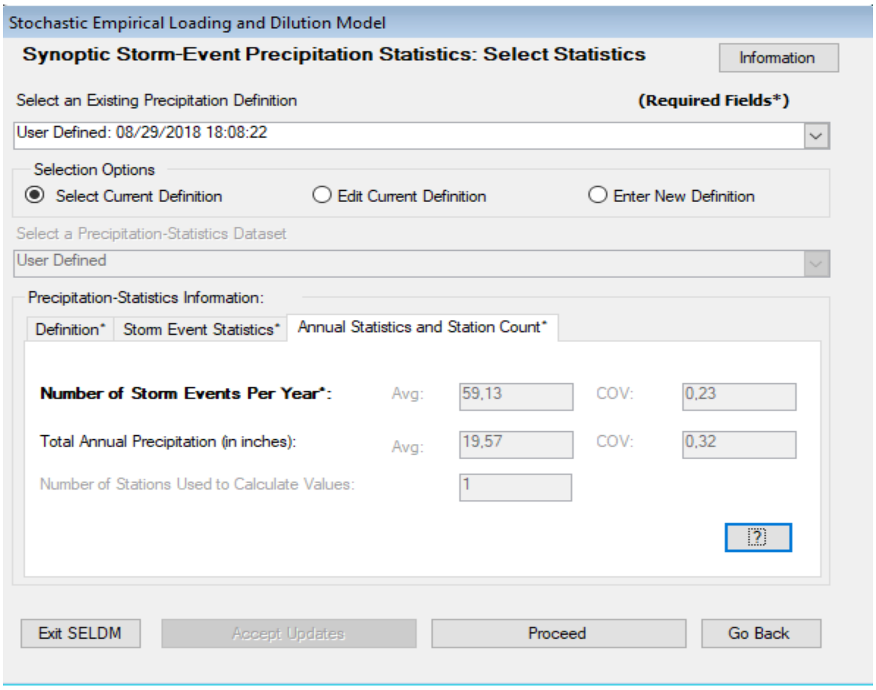
User Defined

Precipitation-Statistics Information:

Definition* | Storm Event Statistics* | Annual Statistics and Station Count*

Storm Event Volume, in Inches*:	Avg:	0,33	COV:	0,99
Storm Event Duration, in Hours*:	Avg:	5,58	COV:	0,67
Time Between Storm Events, in Hours*:	Avg:	146,58	COV:	2,14
Minimum Total Storm Volume, in inches*:		0,1		
Minimum Interevent Time (in hours) *:		6		

Figure II.11 – Synoptic storm-event Precipitation statistics form – second tab. It is where the user fills the required data of the precipitation statistics after choosing the option “user defined” in the previous tab.



Stochastic Empirical Loading and Dilution Model

Synoptic Storm-Event Precipitation Statistics: Select Statistics

Select an Existing Precipitation Definition **(Required Fields*)**

User Defined: 08/29/2018 18:08:22

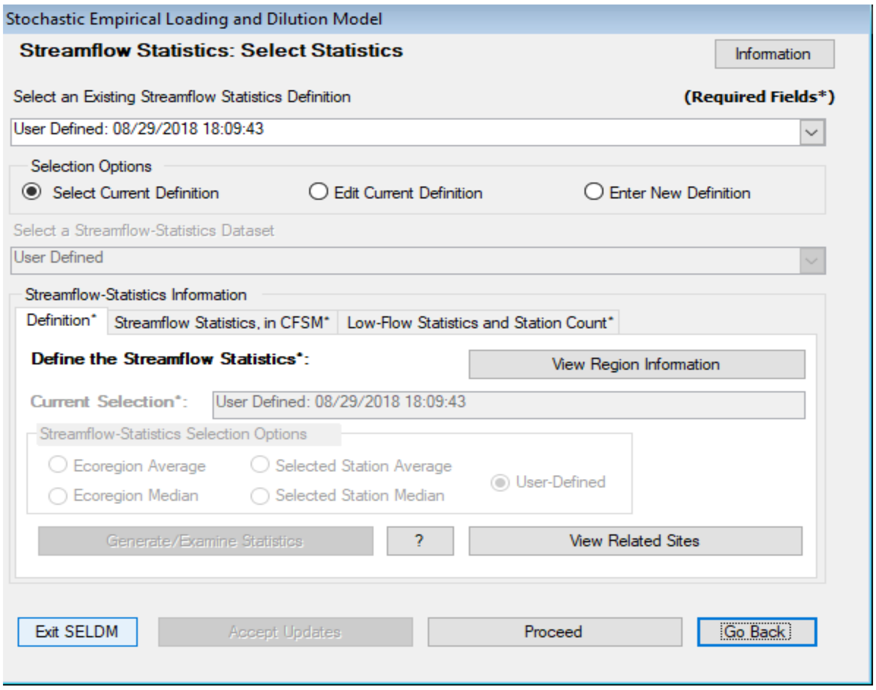
Selection Options
● Select Current Definition ○ Edit Current Definition ○ Enter New Definition

Select a Precipitation-Statistics Dataset: User Defined

Precipitation-Statistics Information:

Number of Storm Events Per Year*:	Avg:	59.13	COV:	0.23
Total Annual Precipitation (in inches):	Avg:	19.57	COV:	0.32
Number of Stations Used to Calculate Values:		1		

Figure II.12 – Synoptic storm-event Precipitation statistics form – third tab. The third and last tab of this form is a continuation of the second.



Stochastic Empirical Loading and Dilution Model

Streamflow Statistics: Select Statistics

Select an Existing Streamflow Statistics Definition **(Required Fields*)**

User Defined: 08/29/2018 18:09:43

Selection Options
● Select Current Definition ○ Edit Current Definition ○ Enter New Definition

Select a Streamflow-Statistics Dataset: User Defined

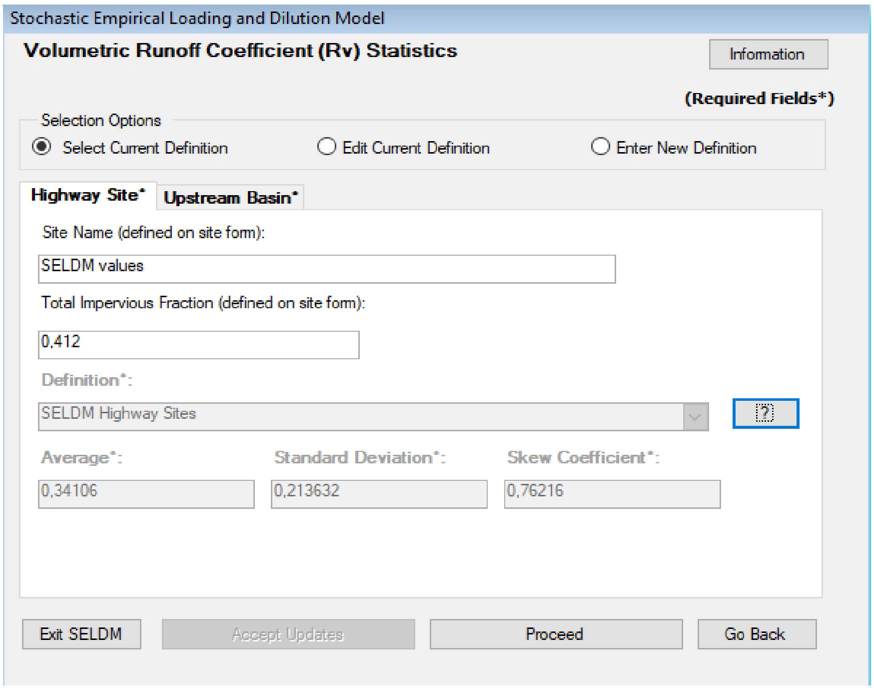
Streamflow-Statistics Information

Define the Streamflow Statistics*:

Current Selection*: User Defined: 08/29/2018 18:09:43

Streamflow-Statistics Selection Options
○ Ecoregion Average ○ Selected Station Average ● User-Defined
○ Ecoregion Median ○ Selected Station Median

Figure II.13 – Streamflow statistics form.



Stochastic Empirical Loading and Dilution Model

Volumetric Runoff Coefficient (Rv) Statistics

(Required Fields*)

Selection Options

● Select Current Definition ○ Edit Current Definition ○ Enter New Definition

Site Name (defined on site form): SELDM values

Total Impervious Fraction (defined on site form): 0,412

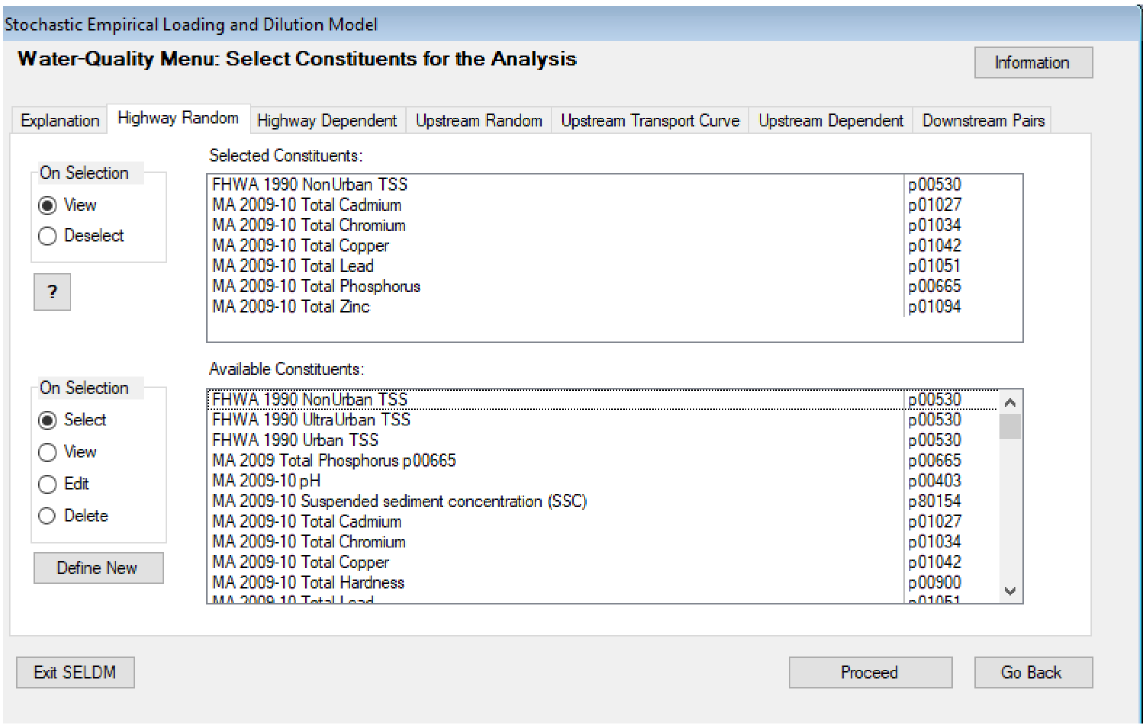
Definition*: SELDM Highway Sites

Average*: 0,34106

Standard Deviation*: 0,213632

Skew Coefficient*: 0,76216

Figure II.14 – Volumetric runoff coefficient statistics form.



Stochastic Empirical Loading and Dilution Model

Water-Quality Menu: Select Constituents for the Analysis

On Selection

● View
○ Deselect

Selected Constituents:

FHWA 1990 NonUrban TSS	p00530
MA 2009-10 Total Cadmium	p01027
MA 2009-10 Total Chromium	p01034
MA 2009-10 Total Copper	p01042
MA 2009-10 Total Lead	p01051
MA 2009-10 Total Phosphorus	p00665
MA 2009-10 Total Zinc	p01094

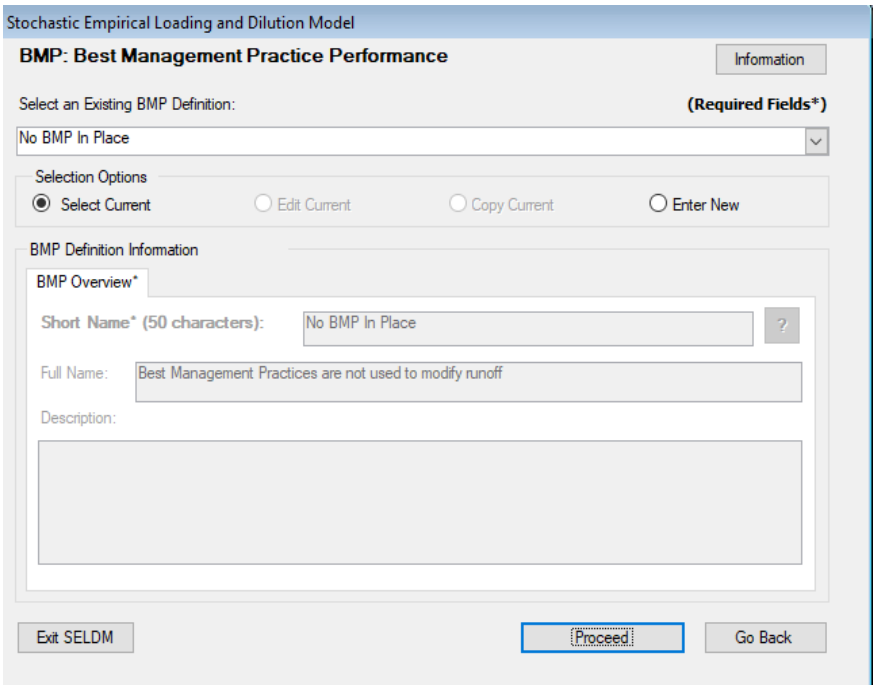
On Selection

● Select
○ View
○ Edit
○ Delete

Available Constituents:

FHWA 1990 NonUrban TSS	p00530
FHWA 1990 UltraUrban TSS	p00530
FHWA 1990 Urban TSS	p00530
MA 2009 Total Phosphorus p00665	p00665
MA 2009-10 pH	p00403
MA 2009-10 Suspended sediment concentration (SSC)	p80154
MA 2009-10 Total Cadmium	p01027
MA 2009-10 Total Chromium	p01034
MA 2009-10 Total Copper	p01042
MA 2009-10 Total Hardness	p00900
MA 2009-10 Total Lead	p01051

Figure II.15 – The water-quality menu form. In this form, the pollutants which will be the output are selected.



BMP: Best Management Practice Performance

Select an Existing BMP Definition: No BMP In Place

(Required Fields*)

Selection Options: ● Select Current ○ Edit Current ○ Copy Current ○ Enter New

BMP Definition Information

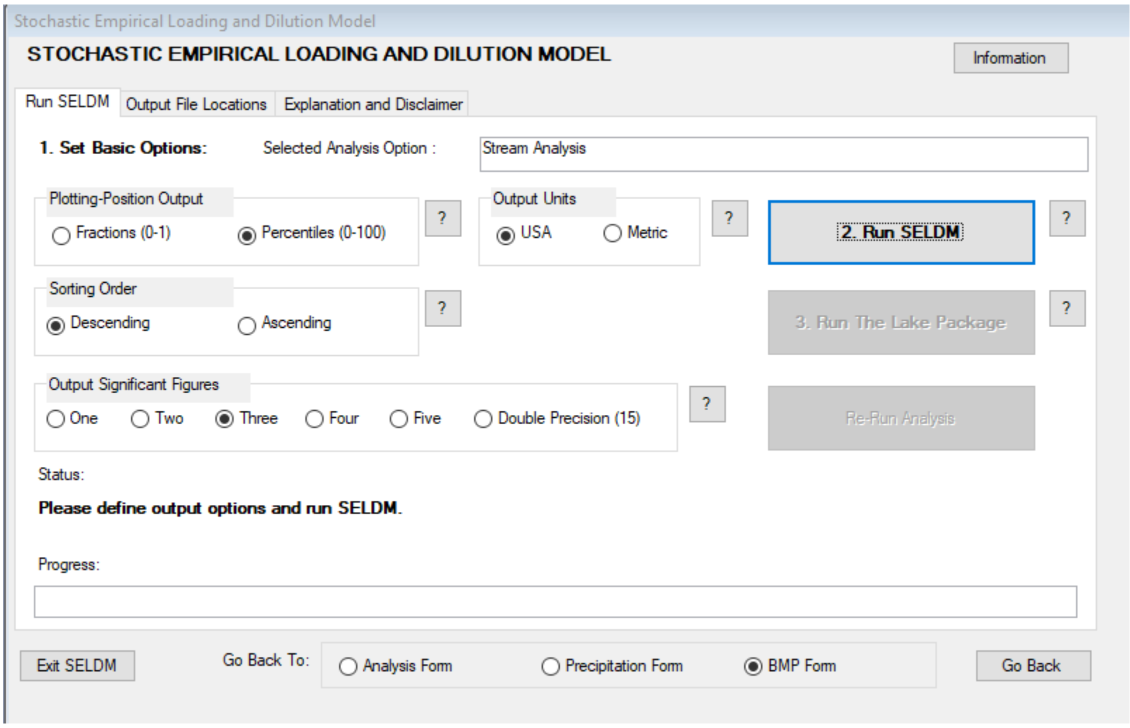
BMP Overview*

Short Name* (50 characters): No BMP In Place

Full Name: Best Management Practices are not used to modify runoff

Description:

Figure II.16 – Best management practice form. This form indicates if the road has any BMP to control the runoff.



STOCHASTIC EMPIRICAL LOADING AND DILUTION MODEL

1. Set Basic Options: Selected Analysis Option : Stream Analysis

Plotting-Position Output: ○ Fractions (0-1) ● Percentiles (0-100)

Output Units: ● USA ○ Metric

Sorting Order: ● Descending ○ Ascending

Output Significant Figures: ○ One ○ Two ● Three ○ Four ○ Five ○ Double Precision (15)

Status:

Please define output options and run SELDM.

Progress:

Go Back To: ○ Analysis Form ○ Precipitation Form ● BMP Form

Figure II.17 – “Running form”. The last form presented in this description is the form where the user runs the model. Here, the user chooses which basic option, significant figures and units of output pretends, to finally run the model.